

Simulating Air Leakage in Walls and Roofs Using Indoor and Outdoor Boundary Conditions

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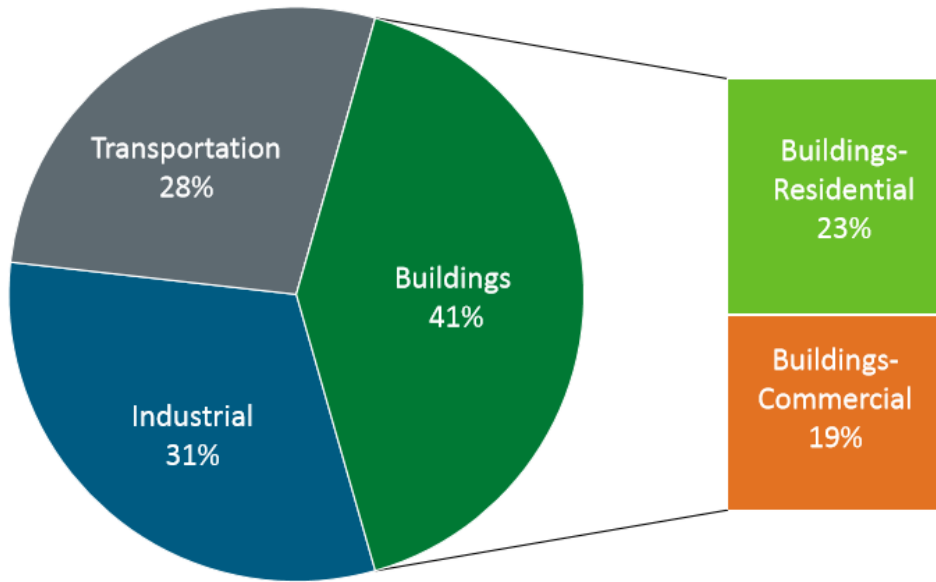
Outline

- Why Reducing Air Leakage Through the Building Envelope?
 - Market Potential
- So What, and Why is Moisture Durability Complicated?
 - Moisture Accumulation
- How Can We Predict the Impact of Air Leakage?
 - Modelling Limitations
 - Simulation Approach
 - Assumptions
- So How Can We Account for Moisture Accumulation?
 - Empirical Formula
 - Example of Usage

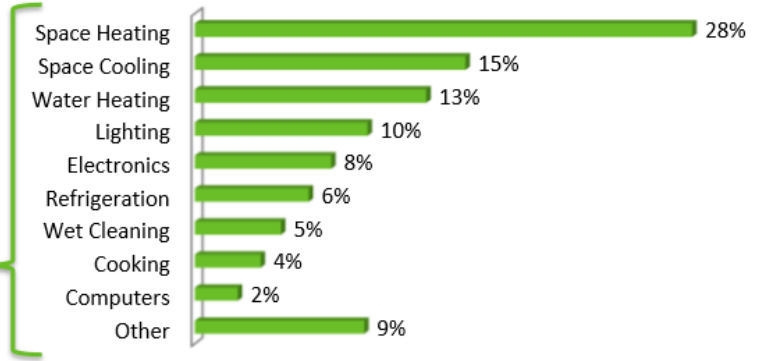
Building Envelope Market Potential



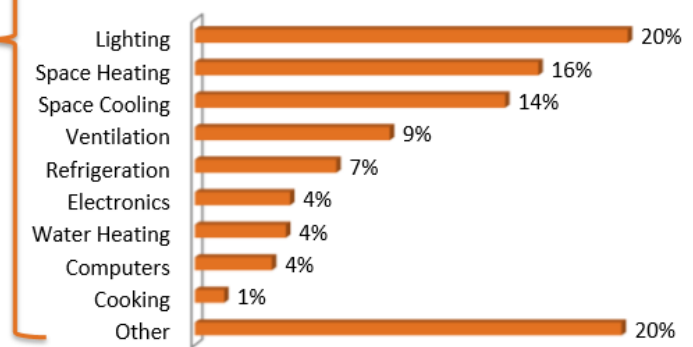
U.S. Primary Energy Consumption
98 Quadrillion Btu



Residential Buildings

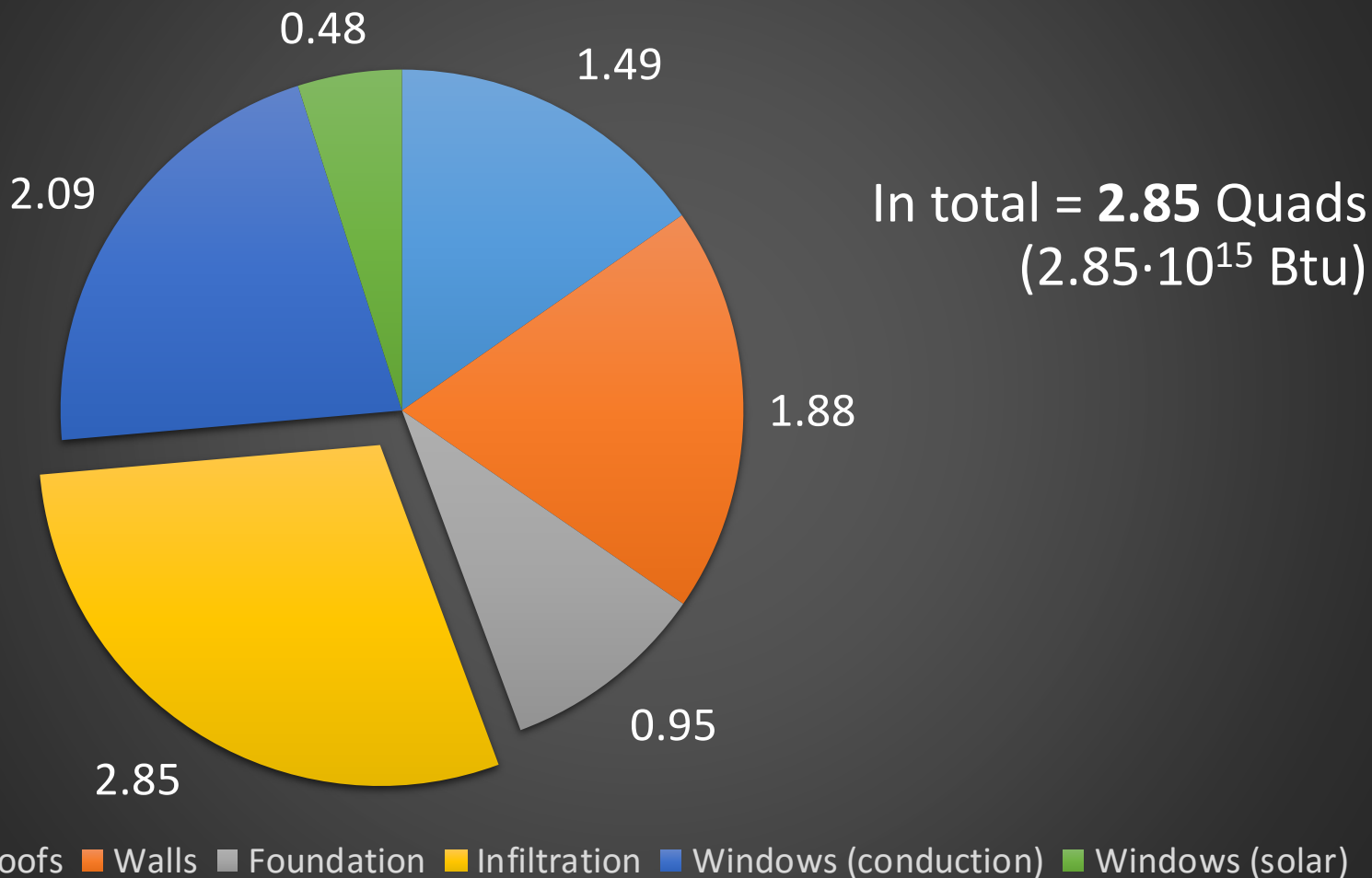


Commercial Buildings



Building Envelope Market Potential

Primary Energy Consumption in Residential Buildings Attributable to Fenestration and Building Envelope Components in 2010 (Quads)



Building Envelope Market Potential

Primary Energy Consumption Attributable to Fenestration and Building Envelope Components for Commercial Buildings in 2010 (Quads)

0.41



103 million tons of coal



~ 490 million barrels of oil

■ Roofs

■ Infiltration

■ Walls

■ Windows (conduction)

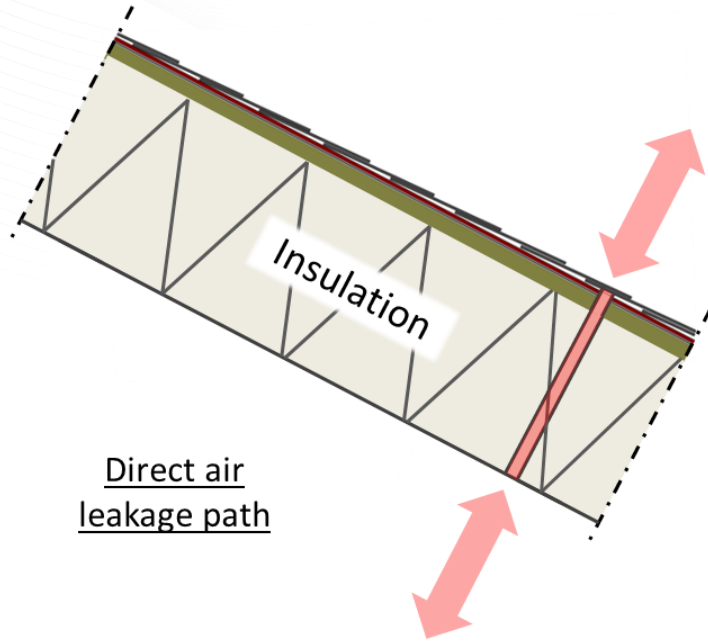
■ Foundation

■ Windows (solar)

Moisture Accumulation

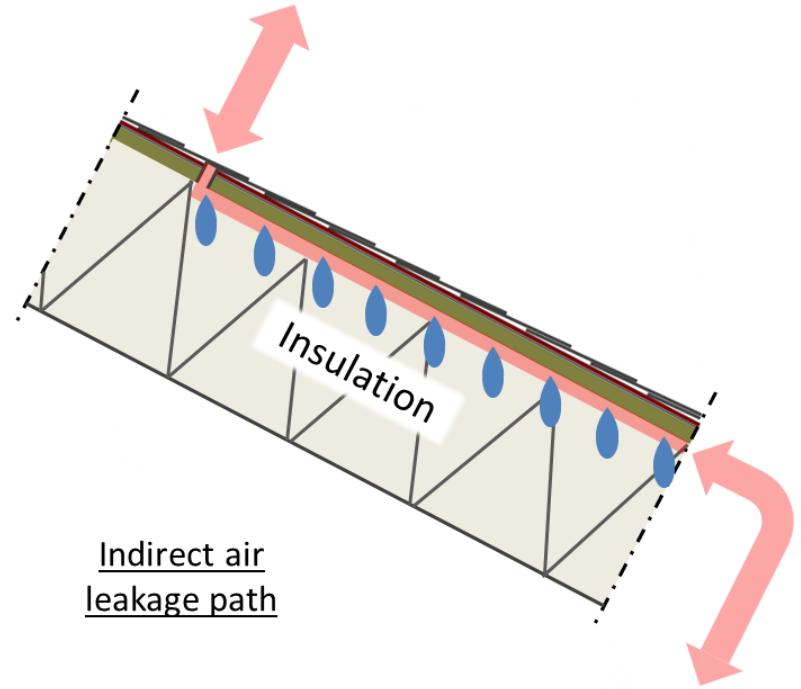


Moisture Accumulation



Direct air leakage path

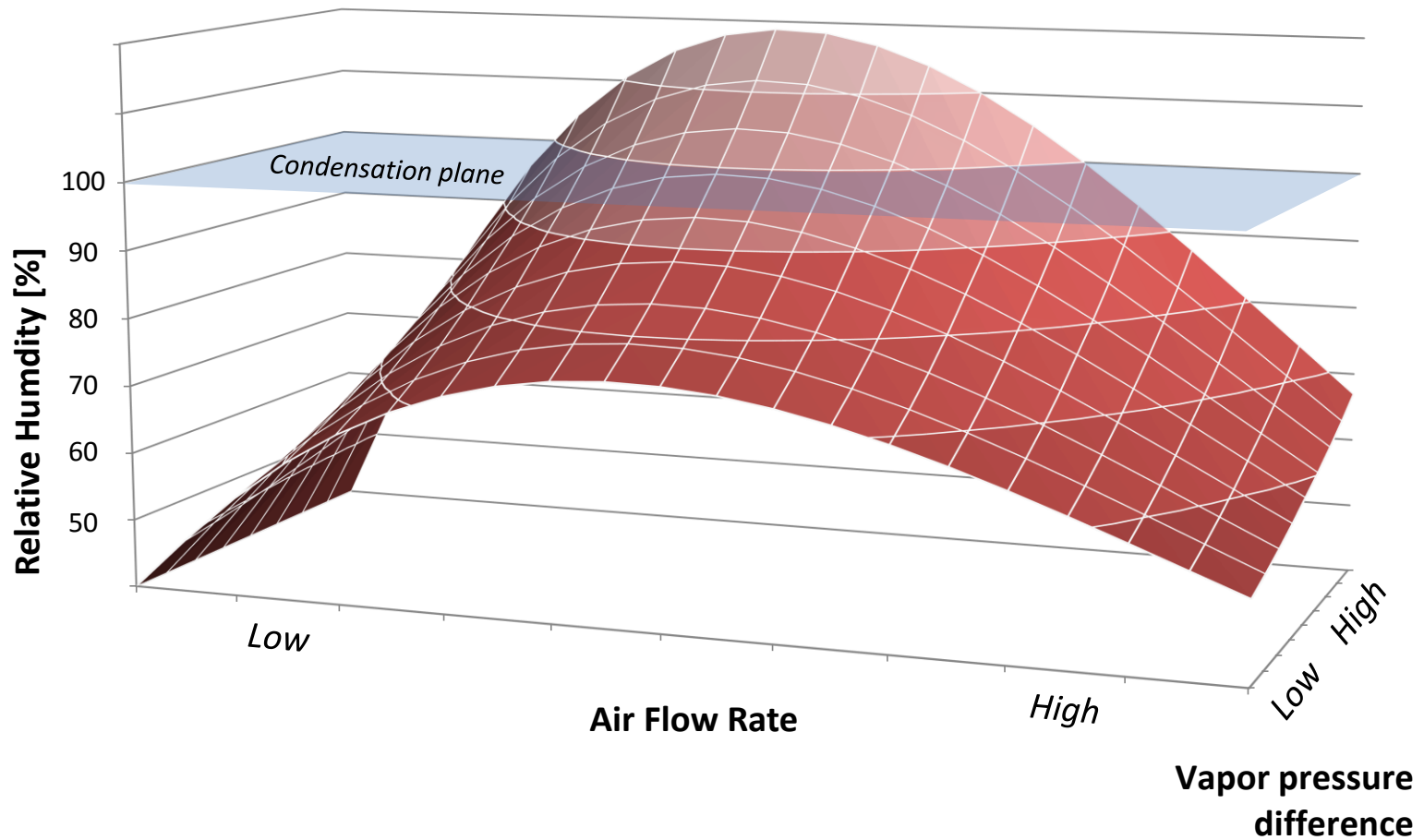
“Energy Leak”



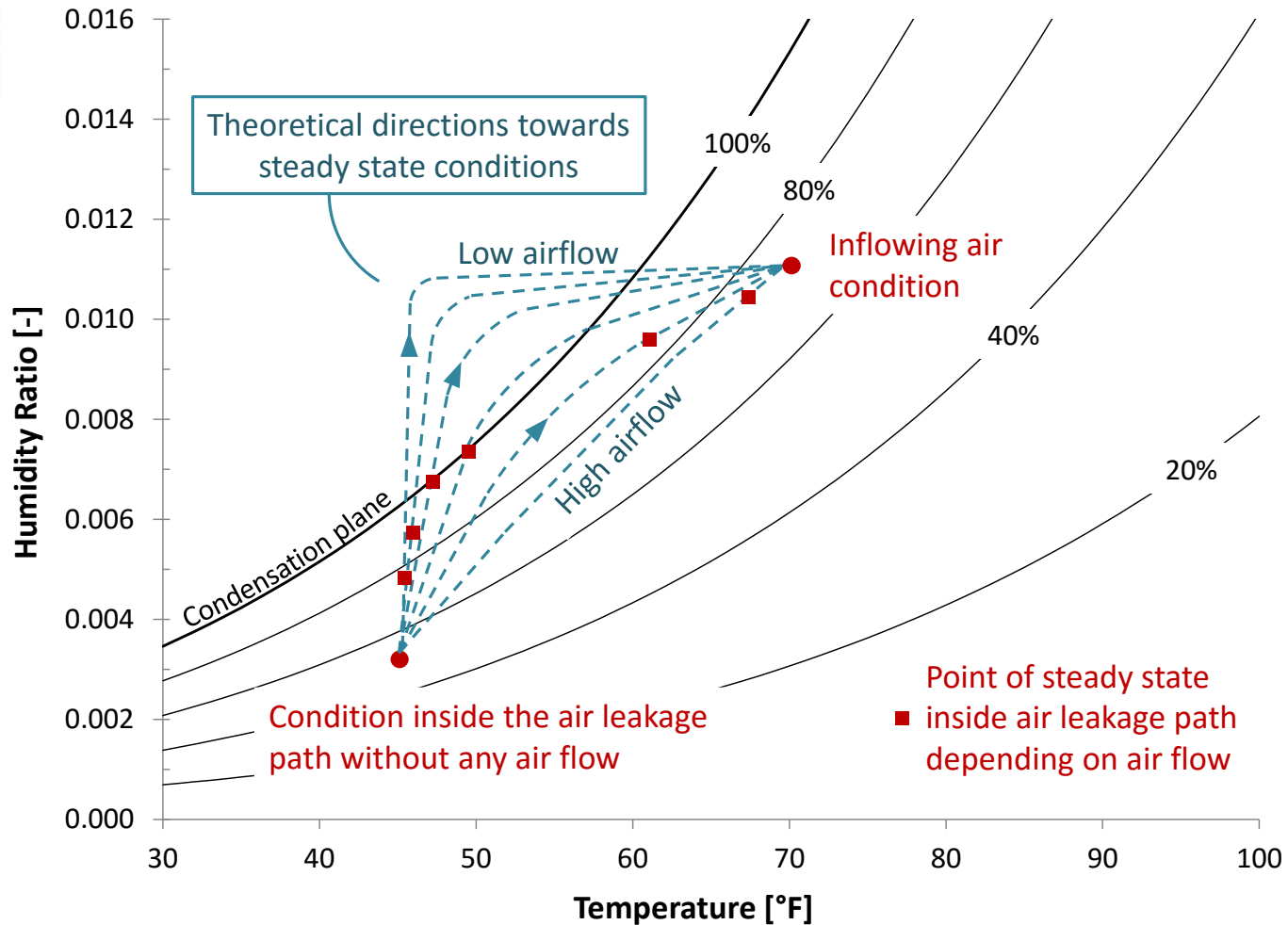
Indirect air leakage path

“Moisture Leak”

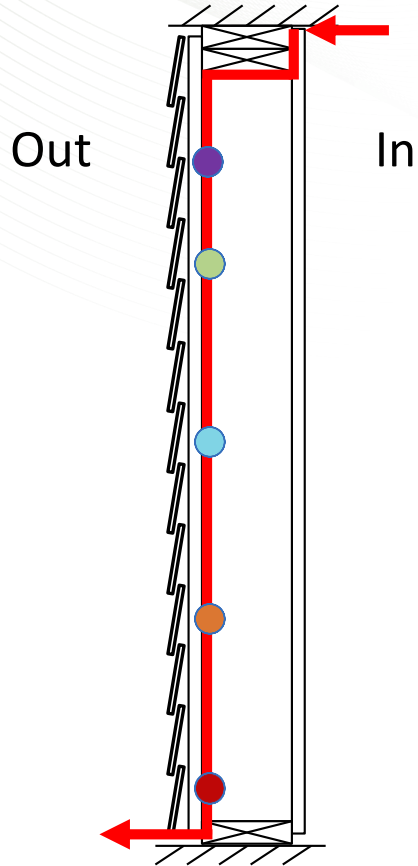
Moisture Accumulation



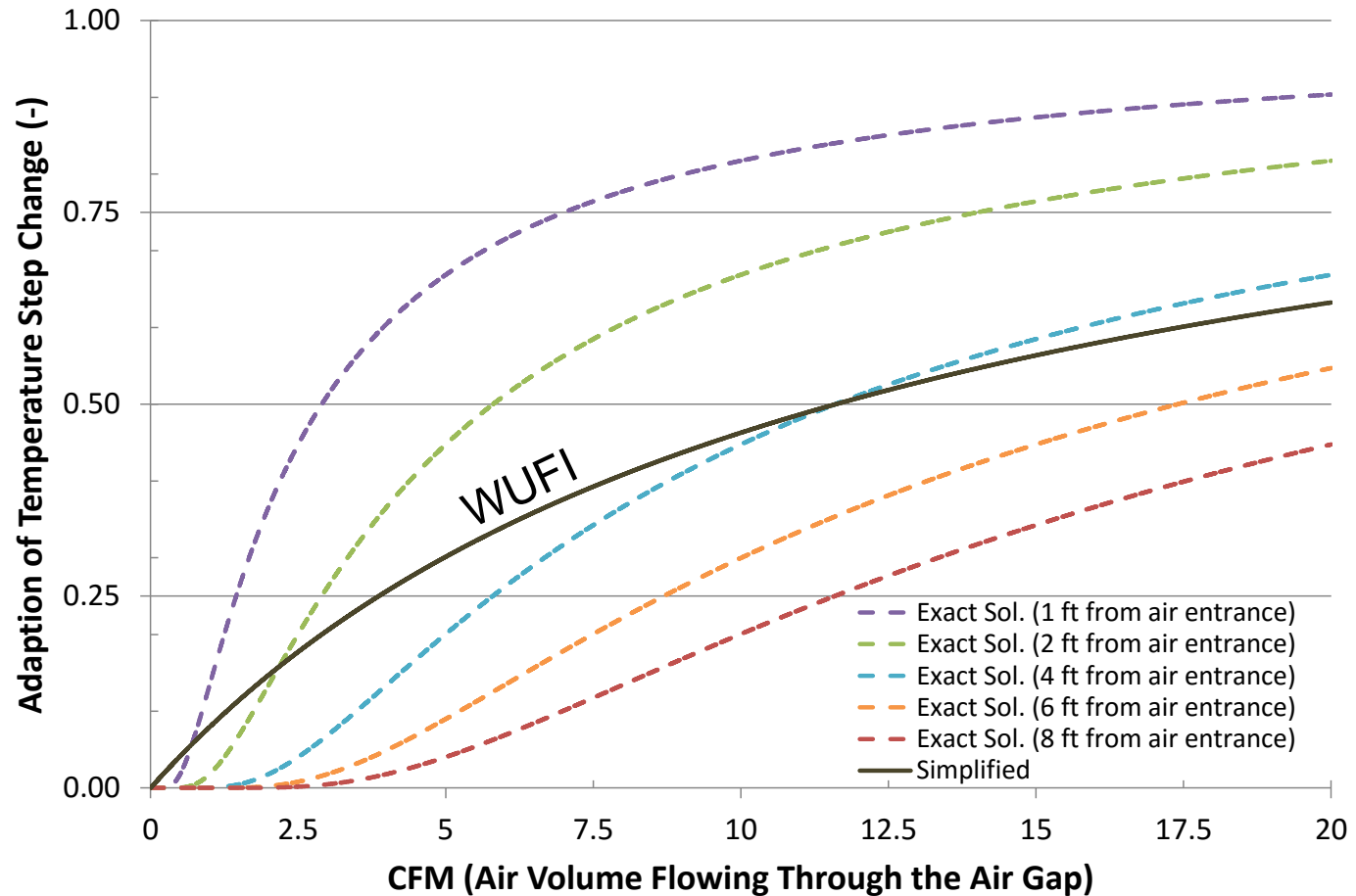
Moisture Accumulation



Modelling Limitations



Exact vs. Simplified Steady State Solutions for Heat Exchange in an Air Channel - Adaption of Step Change

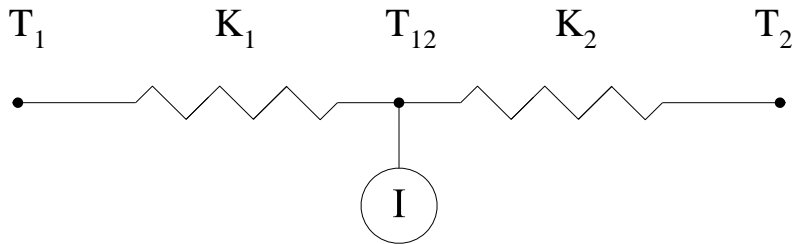


Simulation Approach

1D Solution

$$T_{12}(I) = \frac{\left(T_1 + \frac{I}{K_1}\right) \cdot K_1 + T_2 \cdot K_2}{K_1 + K_2}$$

$$I = \rho_{air} \cdot c_{air} \cdot (T_2 - T_{12}(I)) \cdot \dot{Q}$$



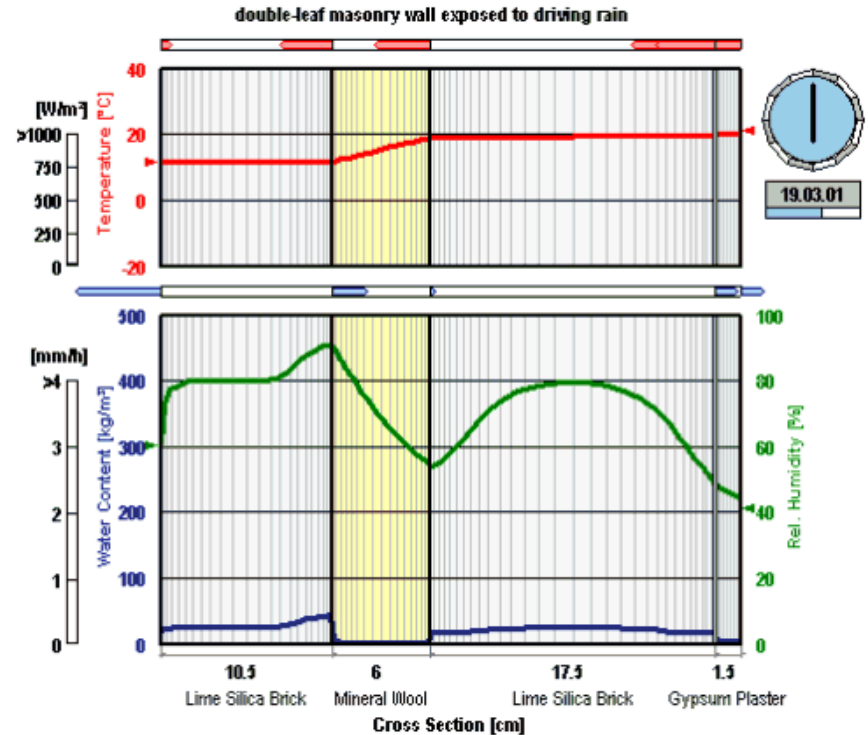
2D Solution

$$T(x) = T_1 + (T_2 - T_1) \cdot e\left(\frac{-x}{l_c}\right)$$

$$l_c = \frac{\rho_{air} \cdot c_{air} \cdot \dot{Q}}{L_{surf} \cdot K}$$

Location: Holzkirchen

WUFI®



Simulation Approach

1D Solution

$$T_{12}(I) = \frac{\left(T_1 + \frac{I}{K_1}\right) \cdot K_1 + T_2 \cdot K_2}{K_1 + K_2}$$

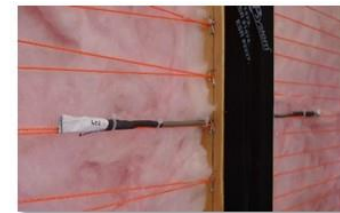
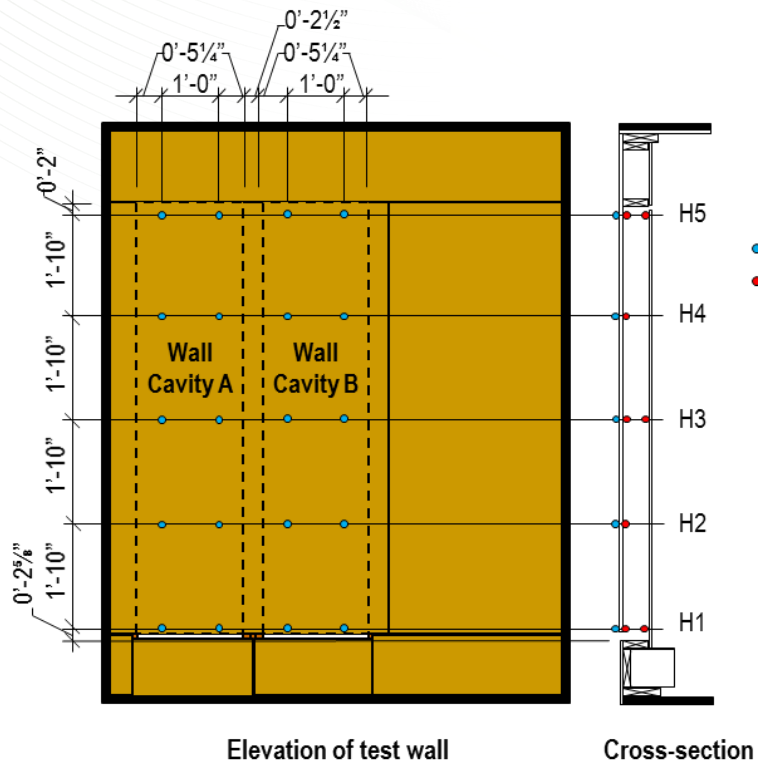
2D Solution

$$T(x) = T_1 + (T_2 - T_1) \cdot e^{\left(\frac{-x}{l_c}\right)}$$

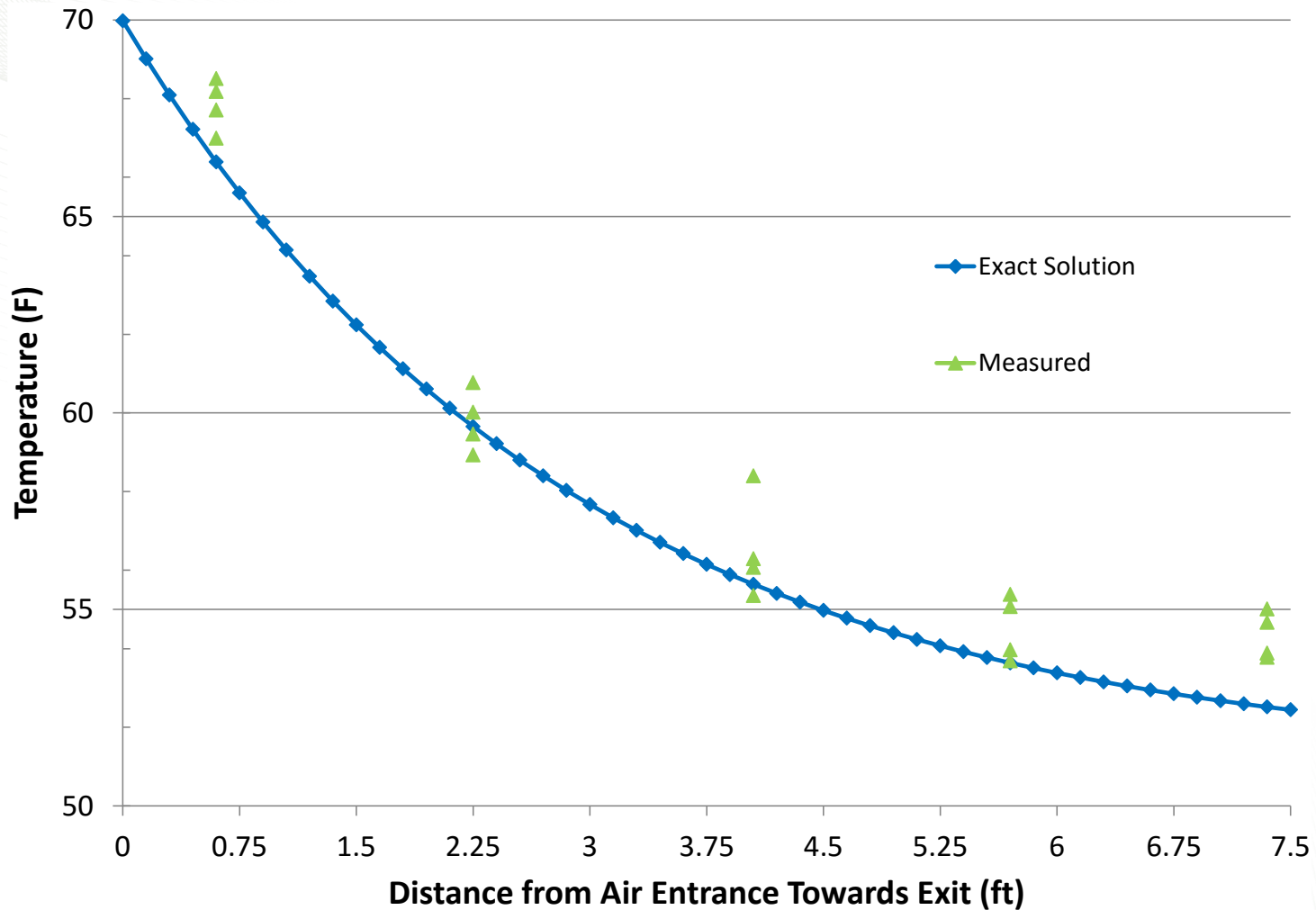
$$\eta = \frac{\left(\frac{T(x) \cdot K - T_2 \cdot K_2}{K_1} - T_1\right) \cdot K_1}{\rho_{air} \cdot c_{air} \cdot (T_2 - T_{12}(I)) \cdot \dot{Q}}$$

$$ACH_{\eta} = \eta(x, \dot{Q}) \cdot ACH$$

Simulation Approach



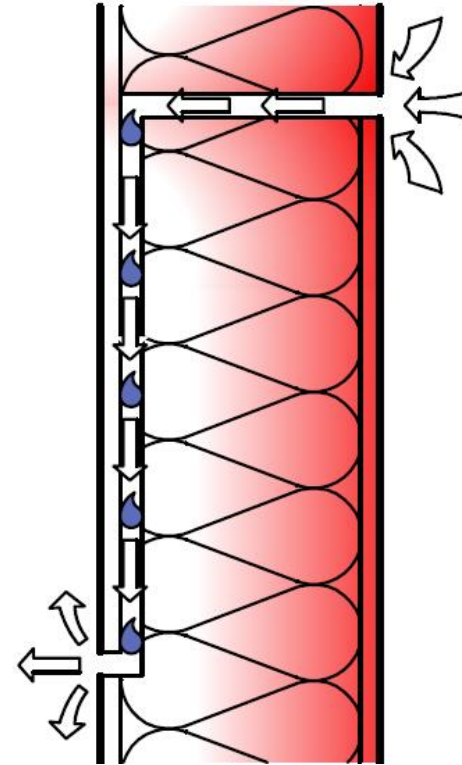
Simulation Approach



Calculated vs. measured steady-state temperatures at a leakage rate of 5.8 cfm (2.7 l/s).

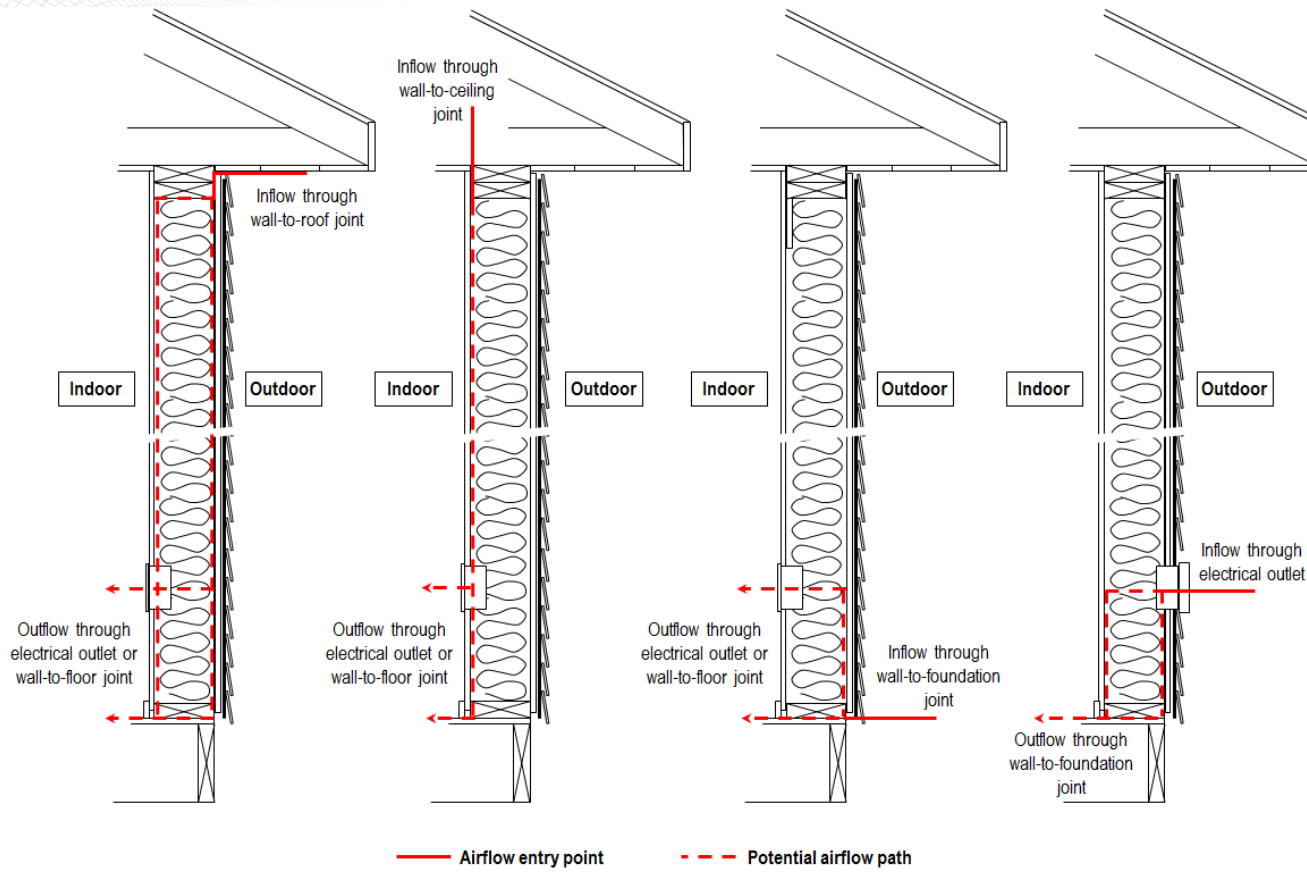
Simulation Approach

- Where are these moisture leaks?
- Flow pattern?

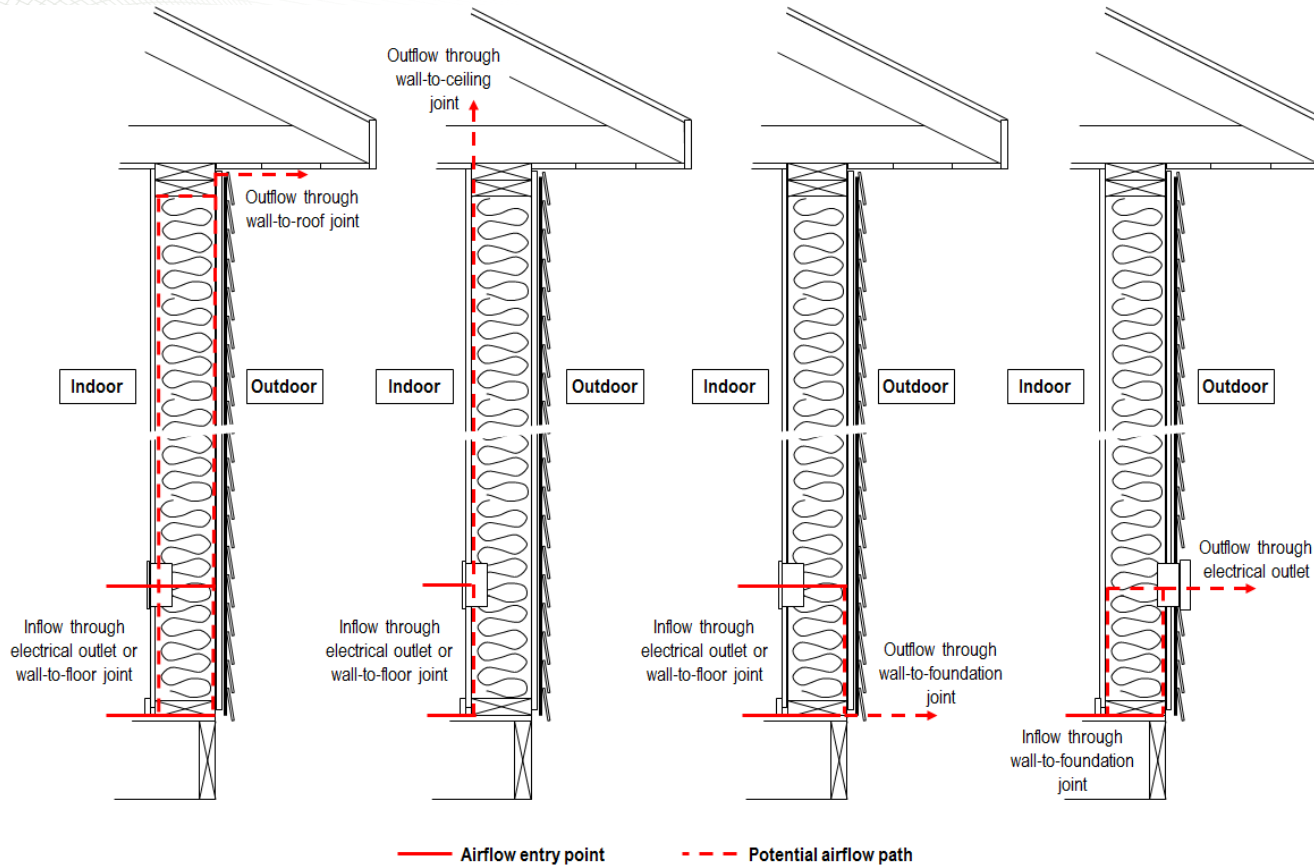


Fraunhofer IBP

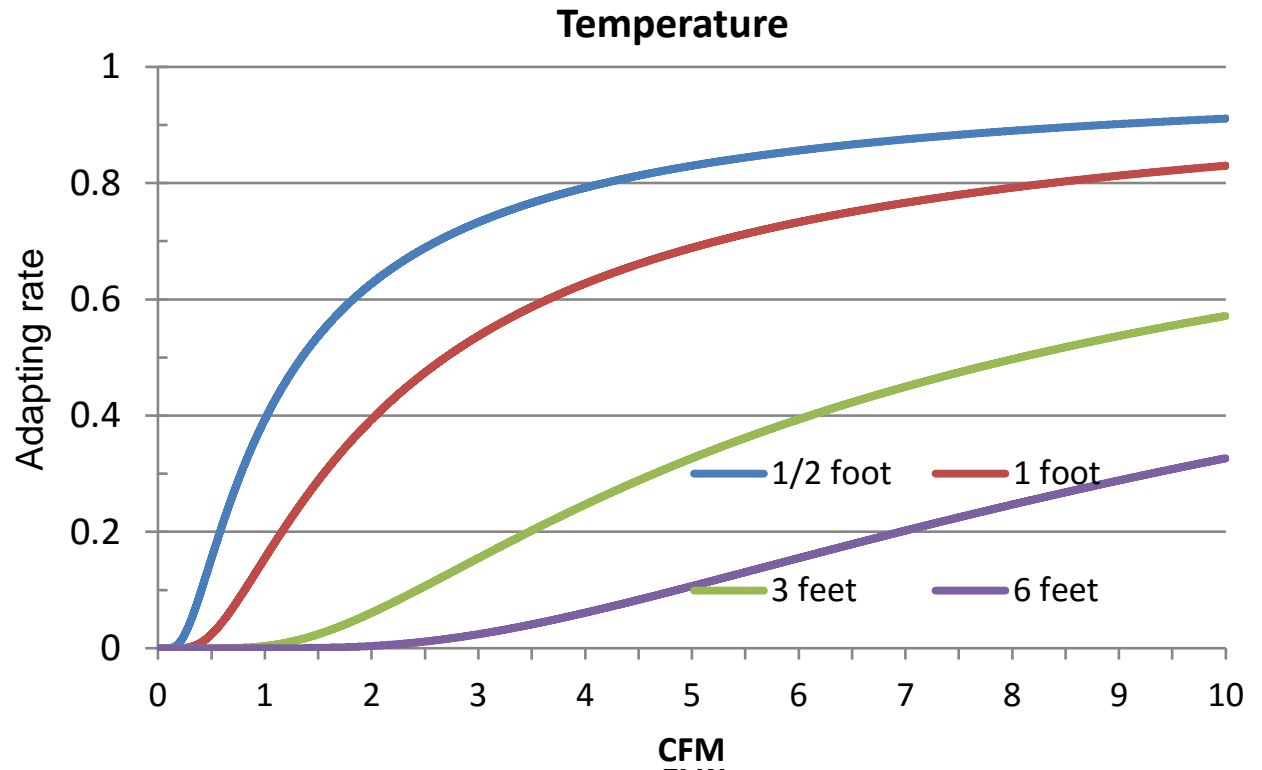
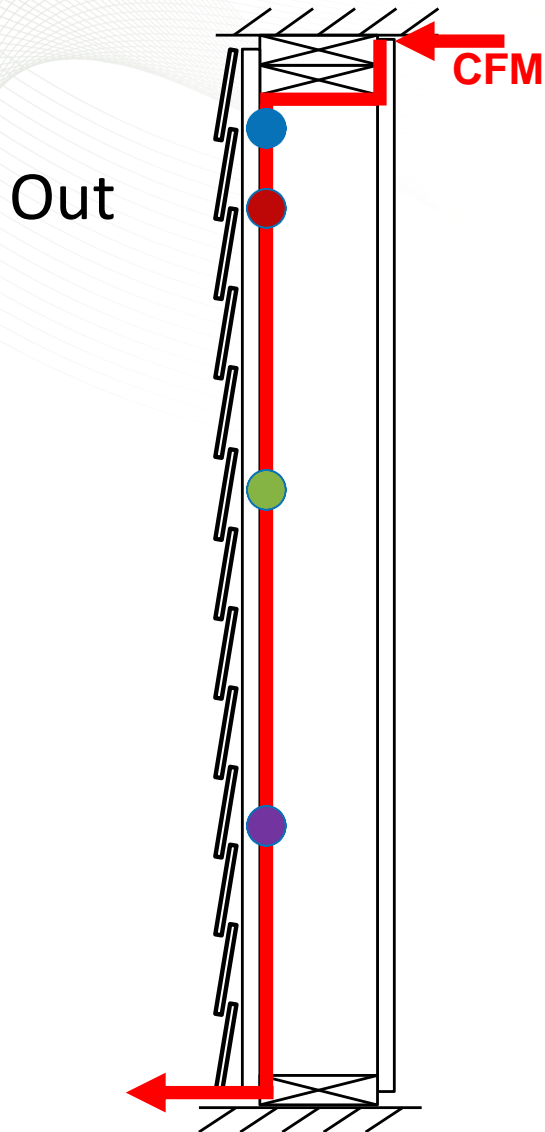
Simulation Approach – Inward Flow



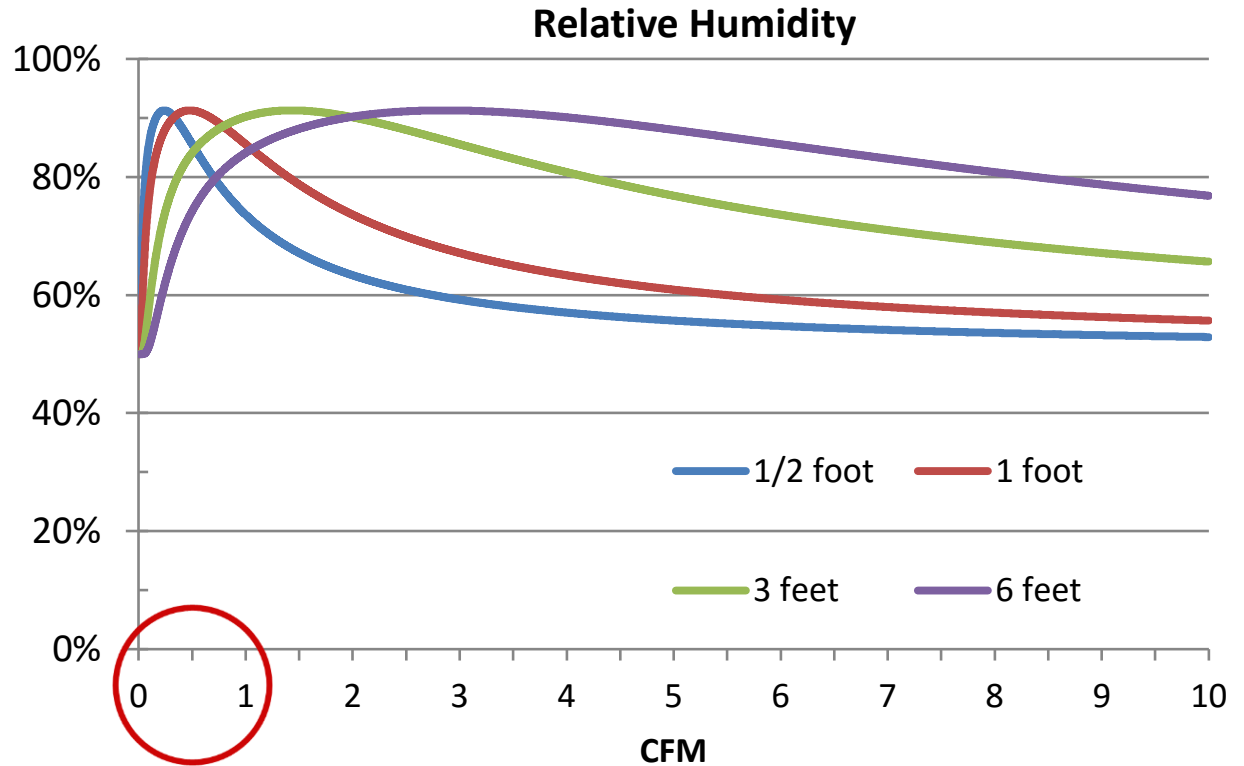
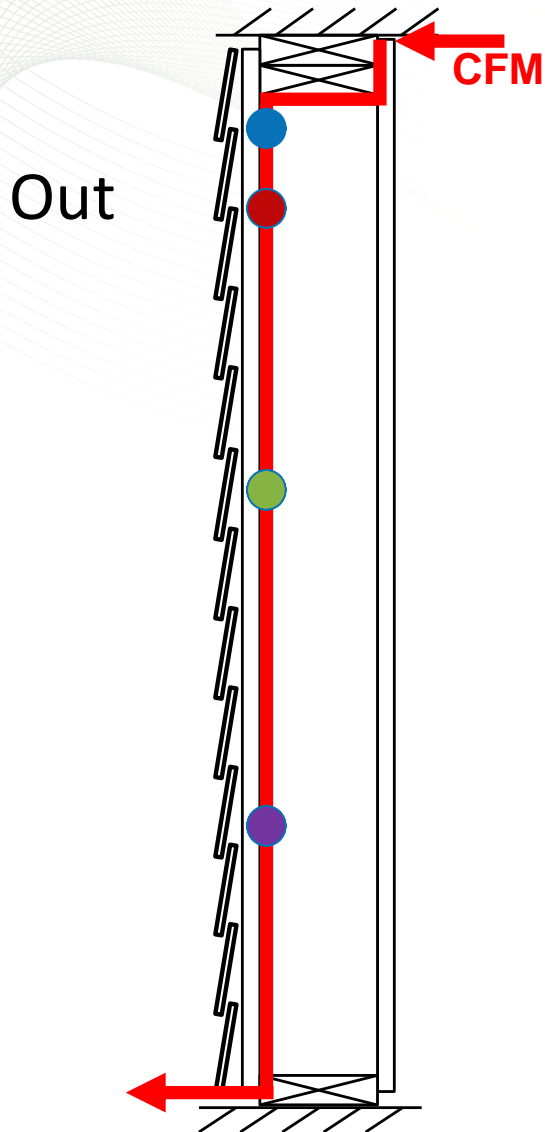
Simulation Approach – Outward Flow



Simulation Approach - Assumption

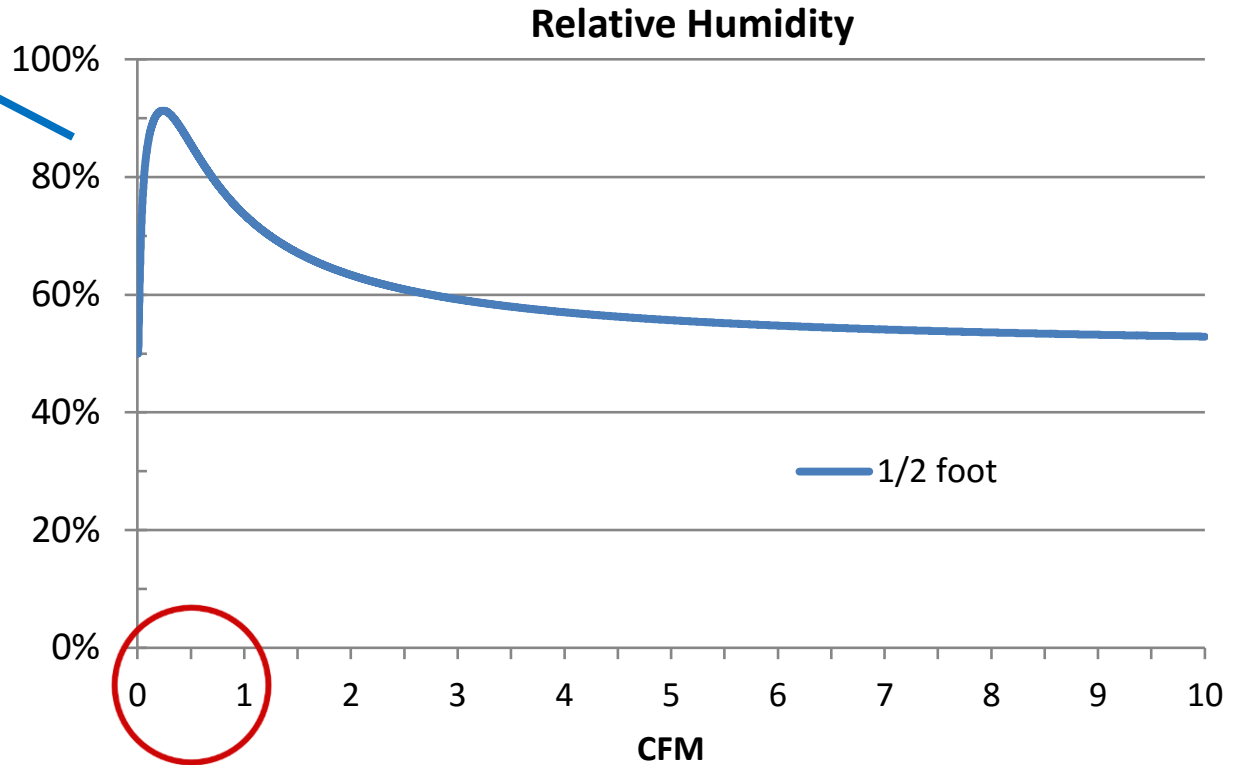
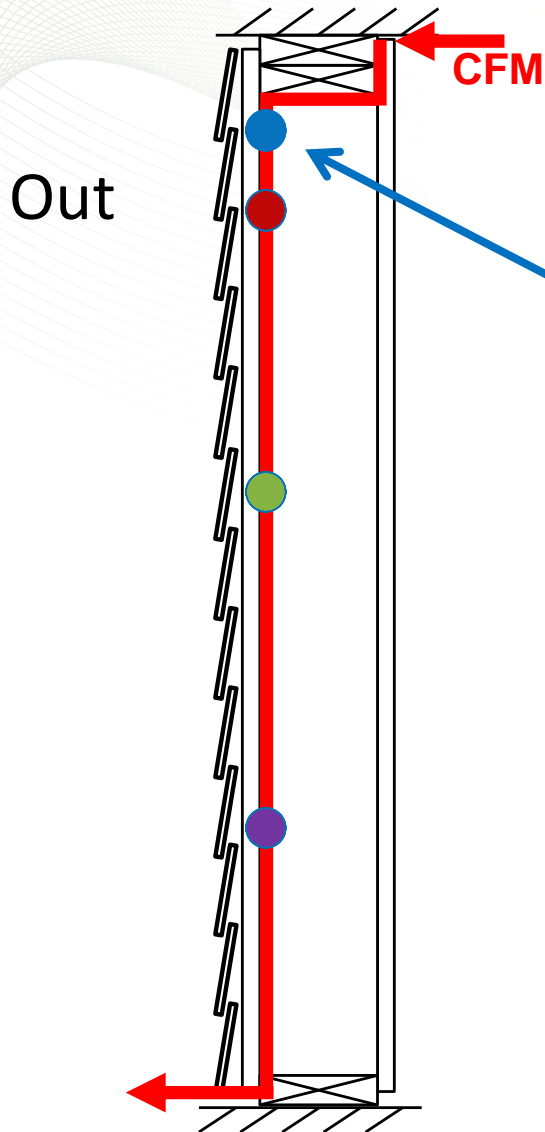


Simulation Approach - Assumption



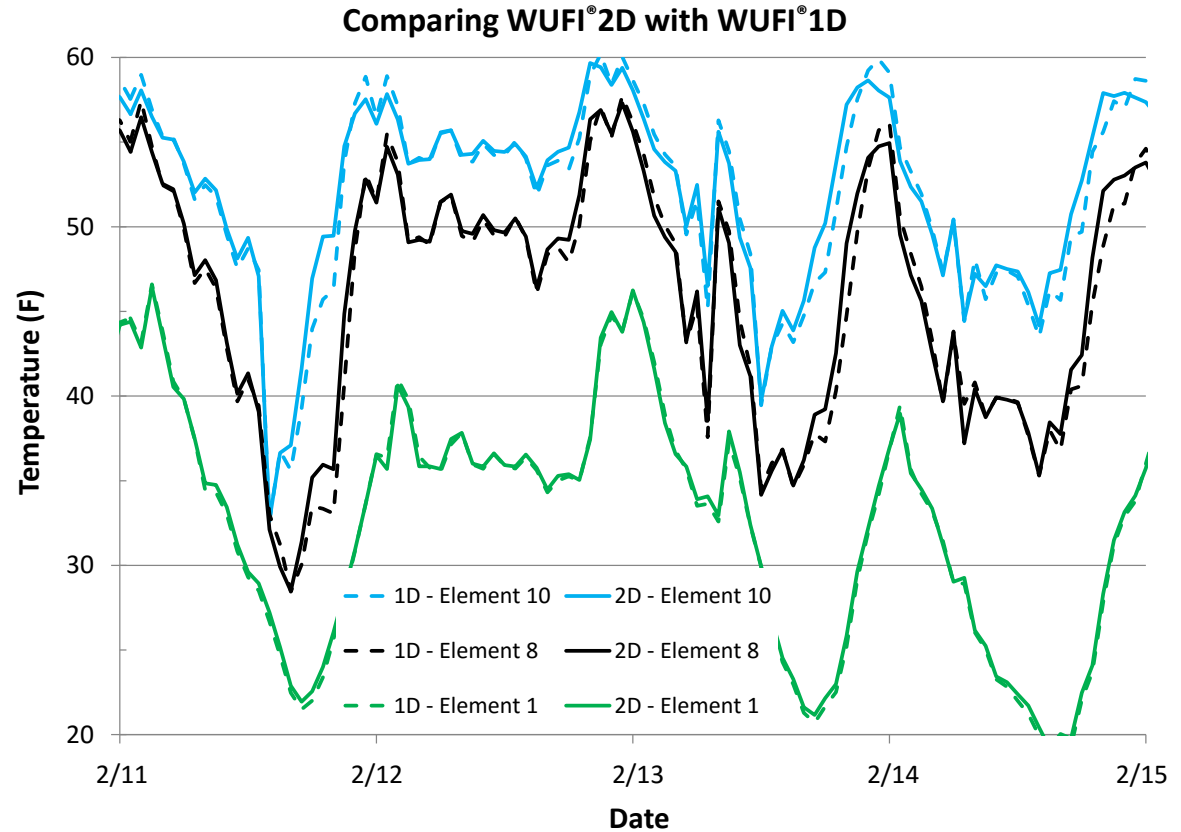
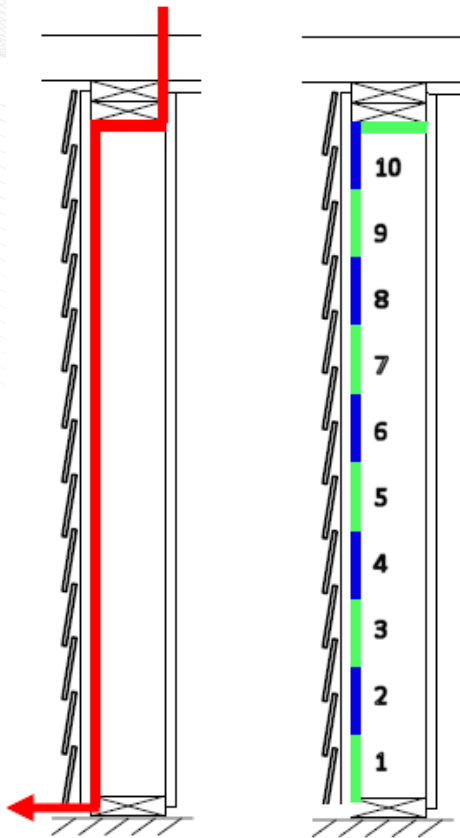
Air flow rates rarely exceed 1 cfm

Simulation Approach - Assumption



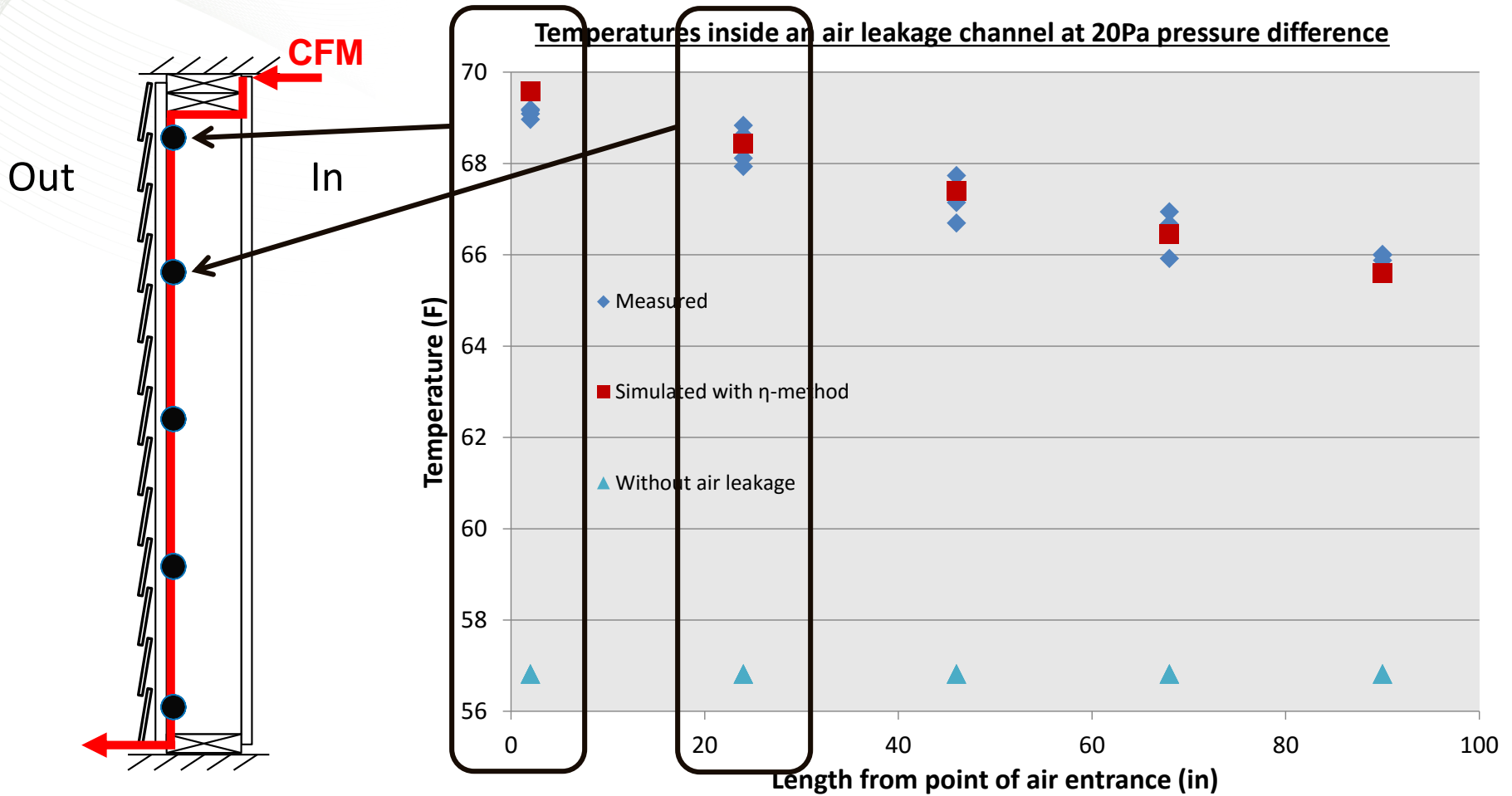
Air flow rates rarely exceed 1 cfm

Simulation Approach - Assumption

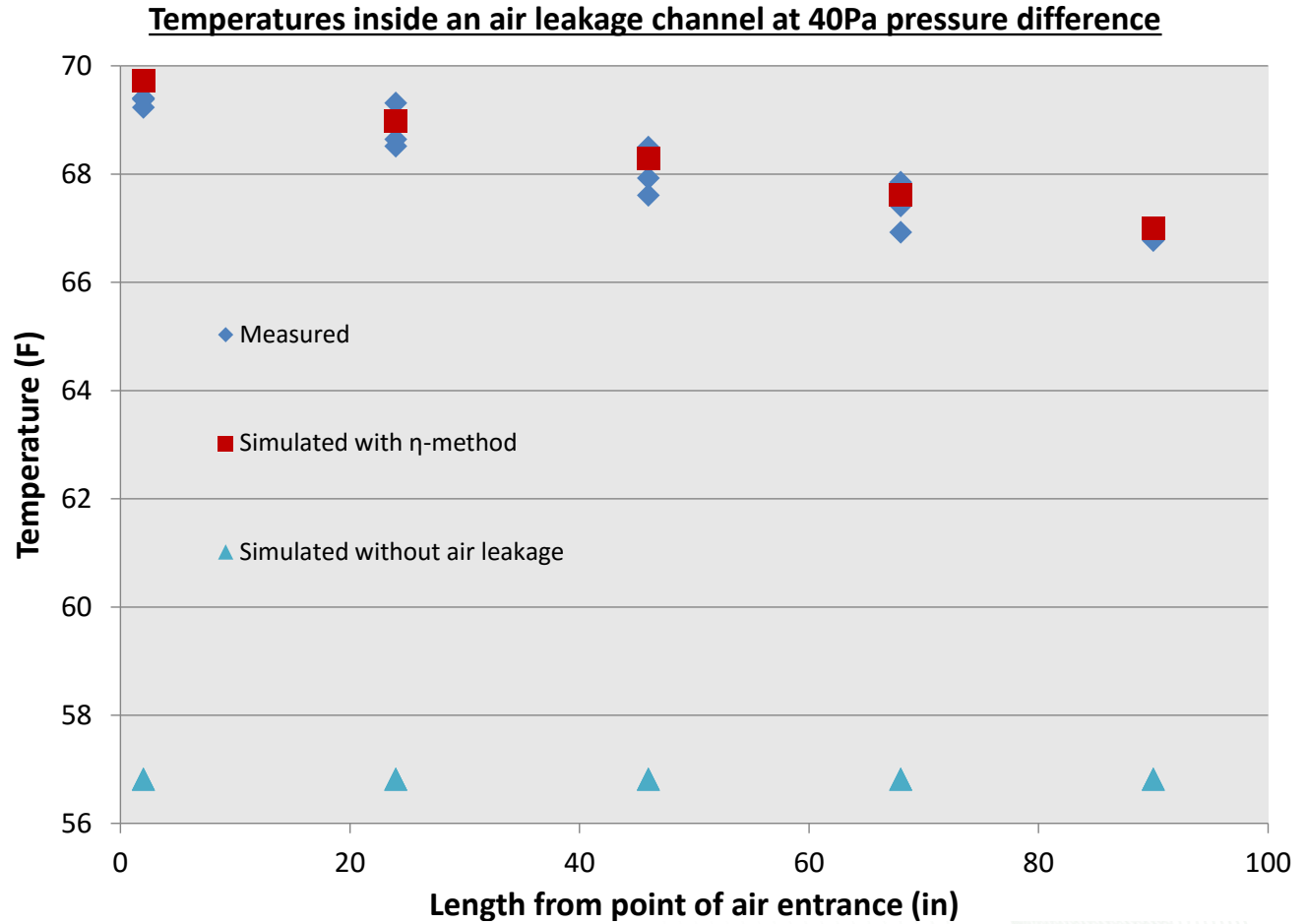
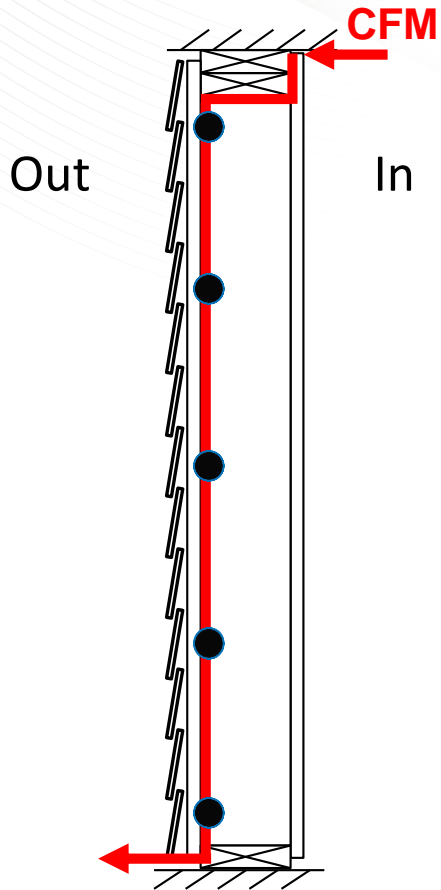


A comparison between WUFI 2D and WUFI 1D reveals that the 1D tool is capable of simulating air leakage at any location inside the air leakage path.

Simulation Approach - Validation



Simulation Approach - Validation



Empirical Formula

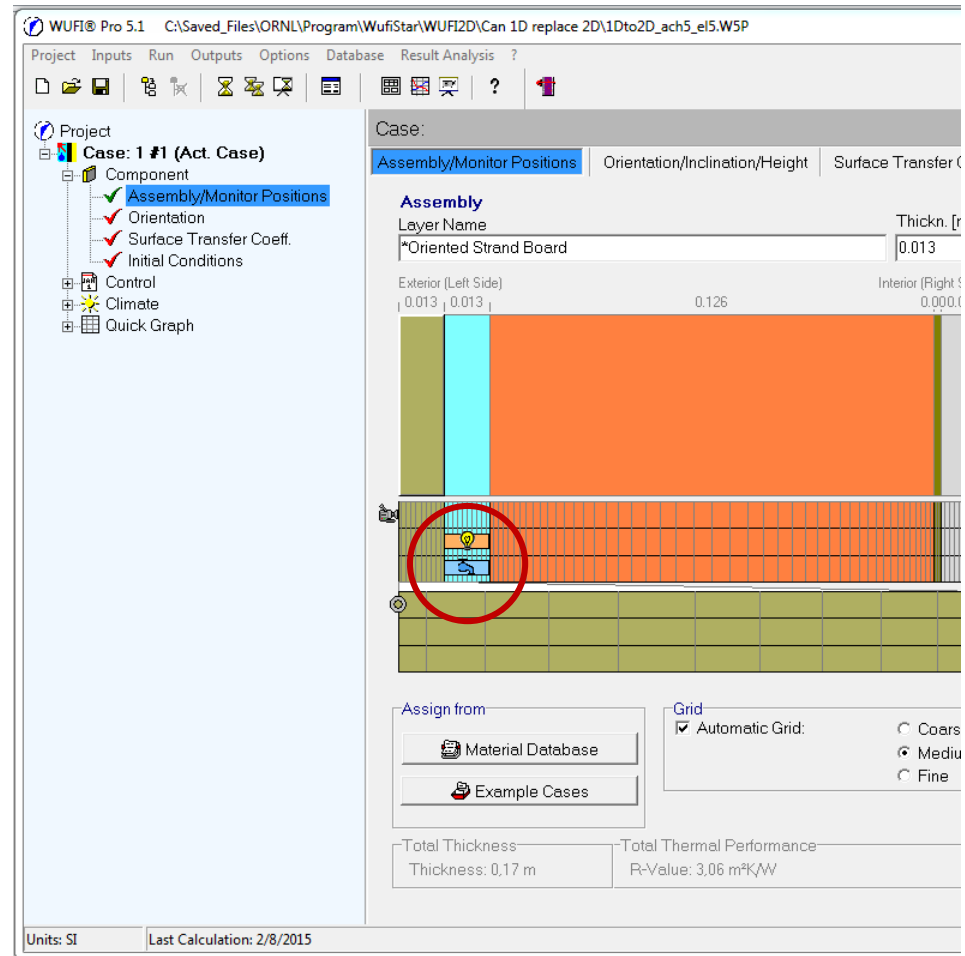
Essential Inputs to account for Air leakage in the Assessment:

- Wind forces
- Wall air tightness
- R -value



Output:

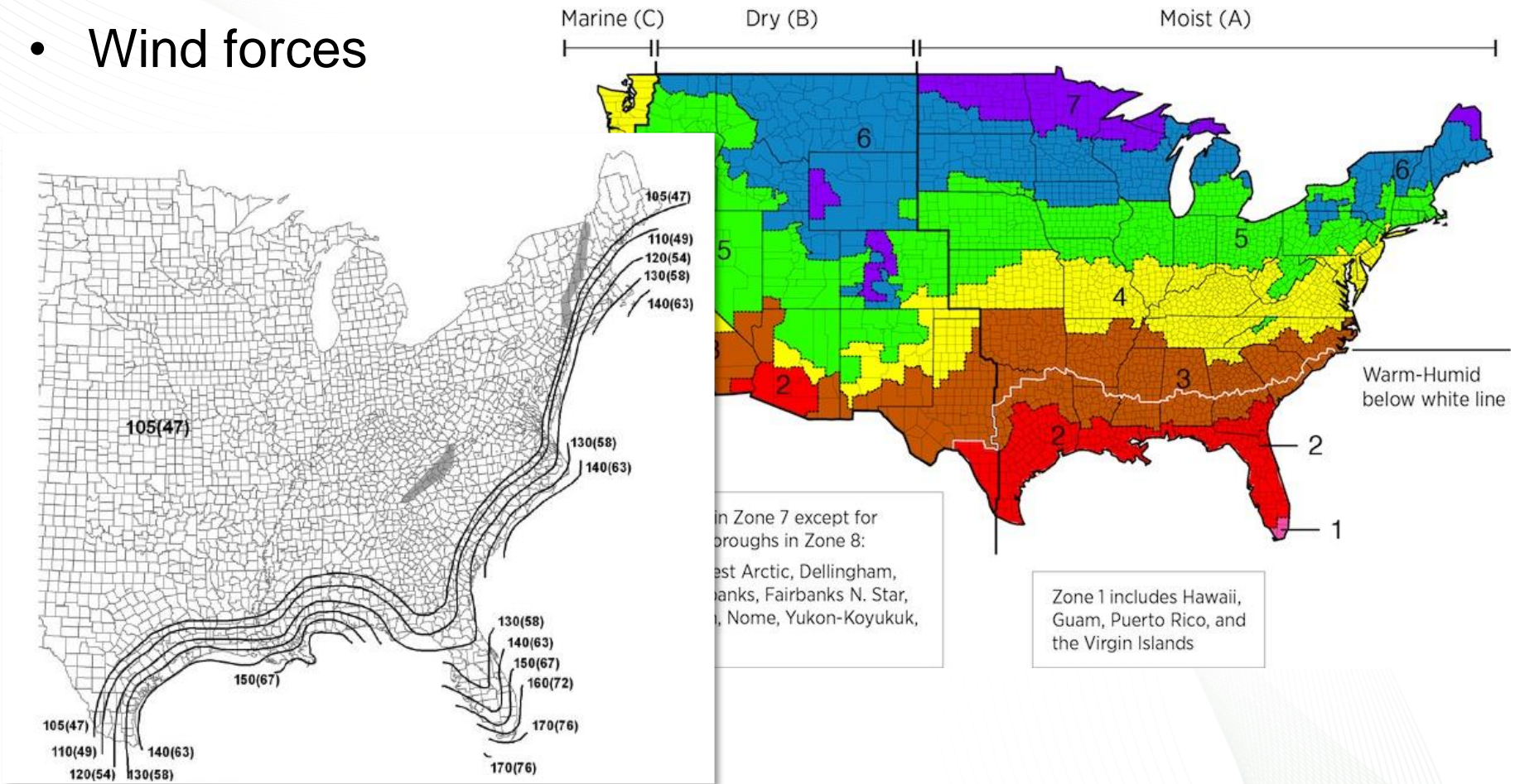
- Air flow rate



Empirical Formula

Essential Inputs to account for Air leakage in the Assessment:

- Wind forces



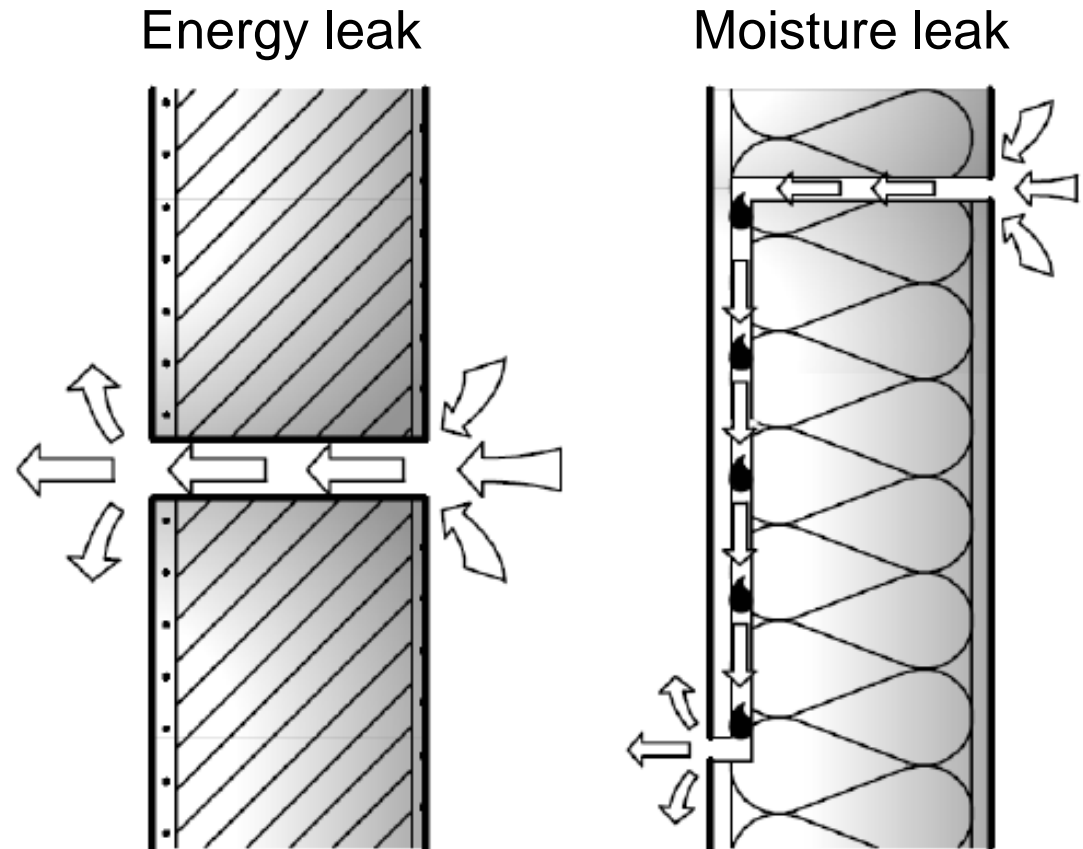
in Zone 7 except for
broughs in Zone 8:
est Arctic, Dellingham,
anks, Fairbanks N. Star,
i, Nome, Yukon-Koyukuk,

Zone 1 includes Hawaii,
Guam, Puerto Rico, and
the Virgin Islands

Empirical Formula

Essential Inputs to account for Air leakage in the Assessment:

- Wall air tightness

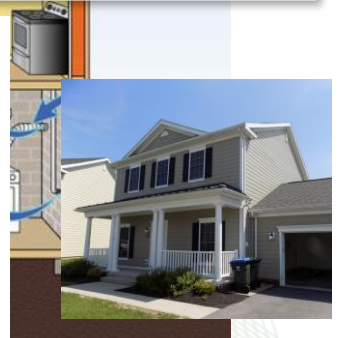
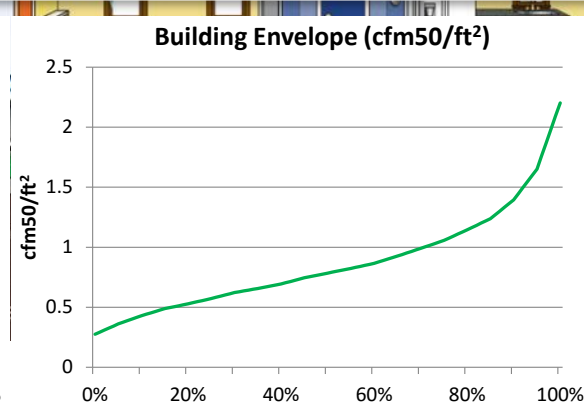
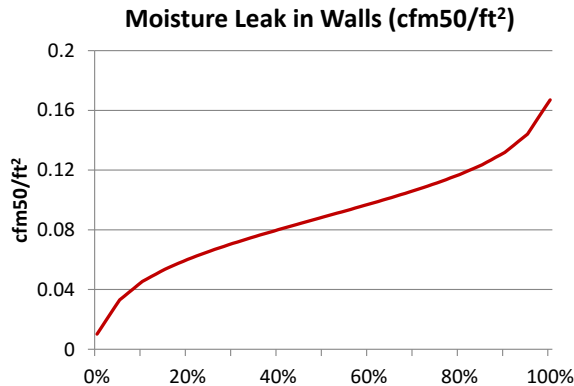
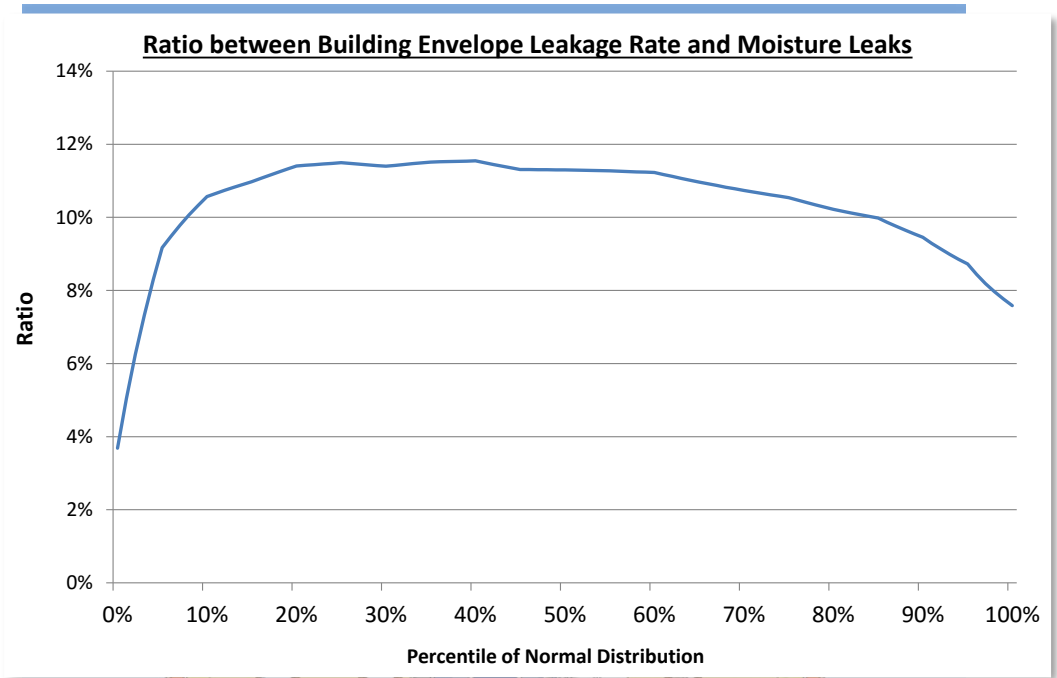
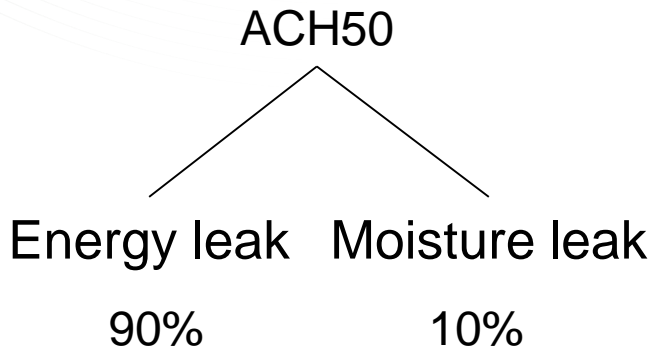


Künzel, H. et.al. (2011). Vapour control design in wooden structures including moisture sources due air exfiltration.

Empirical Formula

Essential Inputs to account for Air leakage in the Assessment:

- Wall air tightness



Empirical Formula

Essential Inputs to account for Air leakage in the Assessment:

- *R*-value

TABLE R402.1.1
INSULATION AND FENESTRATION REQUIREMENTS BY COMPONENT^a

CLIMATE ZONE	FENESTRATION U-FACTOR ^b	SKYLIGHT ^b U-FACTOR	GLAZED FENESTRATION SHGC ^{b, c}	CEILING R-VALUE	WOOD FRAME WALL R-VALUE	MASS WALL R-VALUE ⁱ	FLOOR R-VALUE	BASEMENT ^e WALL R-VALUE	SLAB ^d R-VALUE & DEPTH	CRAWL SPACE ^e WALL R-VALUE
1	NR	0.75	0.25	30	13	3/4	13	0	0	0
2	0.40	0.65	0.25	38	13	4/6	13	0	0	0
3	0.35	0.55	0.25	38	20 or 13+5 ^h	8/13	19	5/13 ^f	0	5/13
4 except Marine	0.35	0.55	0.40	49	20 or 13+5 ^h	8/13	19	10/13	10, 2 ft	10/13
5 and Marine 4	0.32	0.55	NR	49	20 or 13+5 ^h	3/17	30 ^g	15/19	10, 2 ft	15/19
6	0.32	0.55	NR	49	20+5 or 13+10 ^h	5/20	30 ^g	15/19	10, 4 ft	15/19
7 and 8	0.32	0.55	NR	49	20+5 or 13+10 ^h	9/21	38 ^g	15/19	10, 4 ft	15/19

Empirical Formula

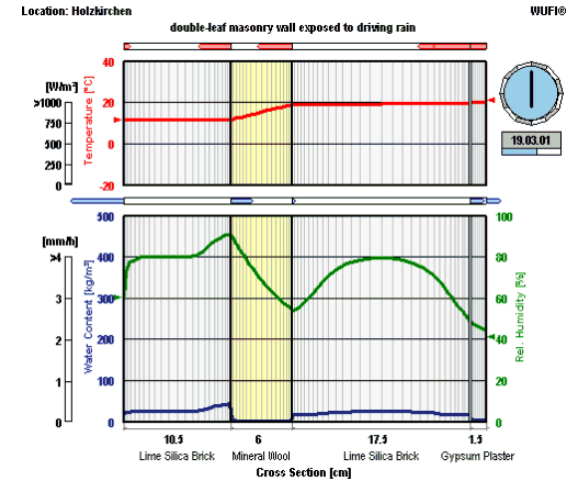
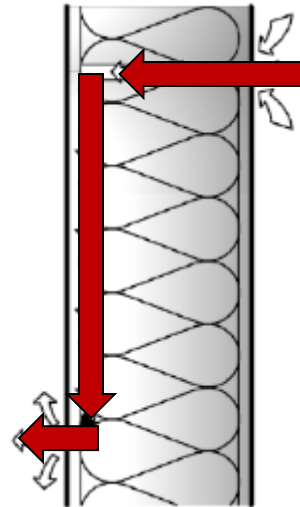
Wind, W (mph)

Wall air tightness, P (cfm/ft²)



Air Flow, Q (cfm)

$Q(W,P)$



Empirical Formula

$$Q = A + B \cdot W + C \cdot P + D \cdot W^2 + E \cdot W \cdot P + F \cdot P^2 \quad (\text{cfm})$$

Example of Usage

$$Q = A + B \cdot W + C \cdot P + D \cdot W^2 + E \cdot W \cdot P + F \cdot P^2 \quad (\text{cfm})$$

Low Range → $W \leq 5 \text{ mph}$

High Range → $W > 5 \text{ mph}$

Example of Usage

$$Q = A + B \cdot W + C \cdot P + D \cdot W^2 + E \cdot W \cdot P + F \cdot P^2 \quad (\text{cfm})$$

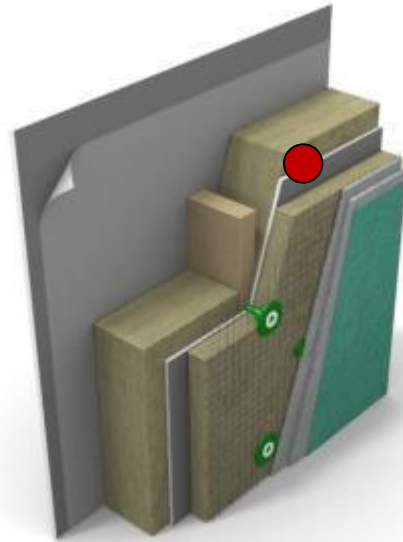
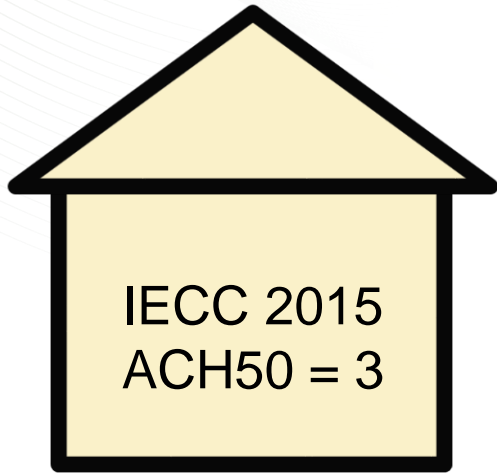
Empirical Factors – Low Range (for $W \leq 5 \text{ mph}$)							
	R-20	R-20 + 3.75	R-20 + 7.5	R-20 + 11.25	R-20 + 15	R-13	R-20 + 5
A	0.0709	-0.0598	-0.0876	-0.0976	-0.1018	0.07215	-0.0661
B	-0.1142	0.01123	0.04161	0.05457	0.06122	-0.1153	0.01777
C	-0.2439	0.18237	0.2744	0.30936	0.32504	-0.2478	0.20294
D	0.02163	0.00329	-0.0015	-0.0037	-0.0049	0.02178	0.00227
E	0.44165	0.28122	0.21963	0.1871	0.1671	0.44241	0.26905
F	0.00751	-0.221	-0.2608	-0.2722	-0.2751	0.00983	-0.2306

Example of Usage

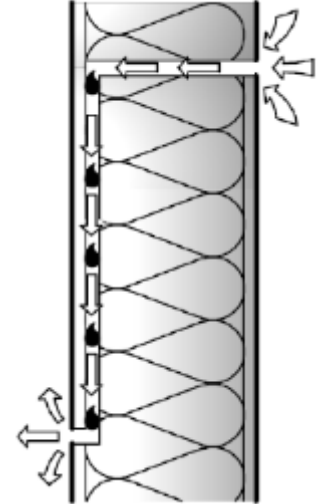
$$Q = A + B \cdot W + C \cdot P + D \cdot W^2 + E \cdot W \cdot P + F \cdot P^2 \quad (\text{cfm})$$

Empirical Factors – High Range (for $W > 5 \text{ mph}$)							
	R-20	R-20 + 3.75	R-20 + 7.5	R-20 + 11.25	R-20 + 15	R-13	R-20 + 5
A	-0.2599	-0.6423	-0.5036	-0.4064	-0.3419	-0.2534	-0.6214
B	0.01469	0.13171	0.1114	0.09502	0.08371	0.013	0.12917
C	0.17613	1.86783	1.73113	1.55883	1.42492	0.15629	1.86376
D	0.00159	-0.0046	-0.0039	-0.0032	-0.0028	0.00167	-0.0045
E	0.50945	0.14144	0.08522	0.06698	0.05897	0.51235	0.12772
F	-0.6499	-1.2146	-1.0939	-0.9842	-0.9032	-0.6422	-1.201

Example of Usage



R-20+5



ACH50 = 3



$P \approx 0.2 \text{ cfm/ft}^2$

Example of Usage

$$Q = A + B \cdot W + C \cdot 0.2 + D \cdot W^2 + E \cdot W \cdot 0.2 + F \cdot 0.2^2$$

Empirical Factors – Low Range (for $W \leq 5$ mph)							
	R-20	R-20 + 3.75	R-20 + 7.5	R-20 + 11.25	R-20 + 15	R-13	R-20 + 5
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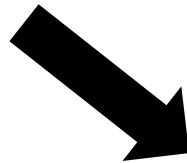
Example of Usage

$$Q = A + B \cdot W + C \cdot 0.2 + D \cdot W^2 + E \cdot W \cdot 0.2 + F \cdot 0.2^2$$

$$Q = -0.0661 + 0.0177 \cdot W + 0.20294 \cdot 0.2 + 0.0023 \cdot W^2 + 0.2691 \cdot W \cdot 0.2 - 0.2603 \cdot 0.2^2$$

$$Q = -0.0347 + 0.0716 \cdot W + 0.0023 \cdot W^2$$

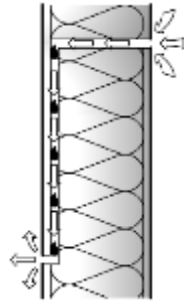
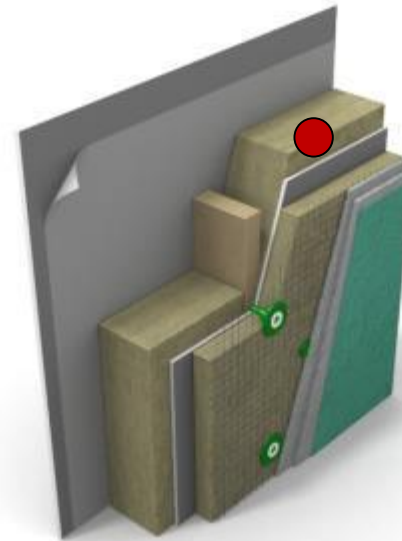
Wind = 5 *mph*



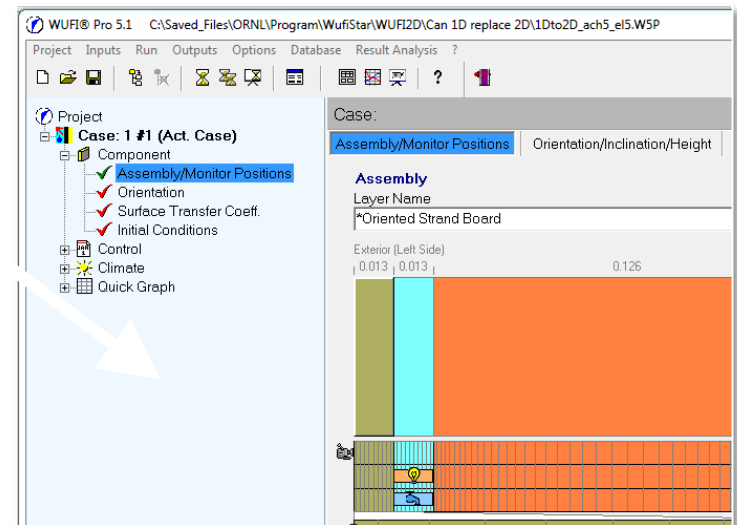
Q = 0.38 *cfm*

Example of Usage

3 ACH50 & R-20+5	
Wind (mph)	Air Leakage (cfm)
0	0
0.1	4.83564E-08
0.2	0.000173
0.3	0.001587
0.4	0.004482
0.5	0.008417
0.6	0.01307
0.7	0.01826
0.8	0.02387
...	...



$$Q = -0.0347 + 0.0716 \cdot W + 0.0023 \cdot W^2$$



Discussion



Contact information

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