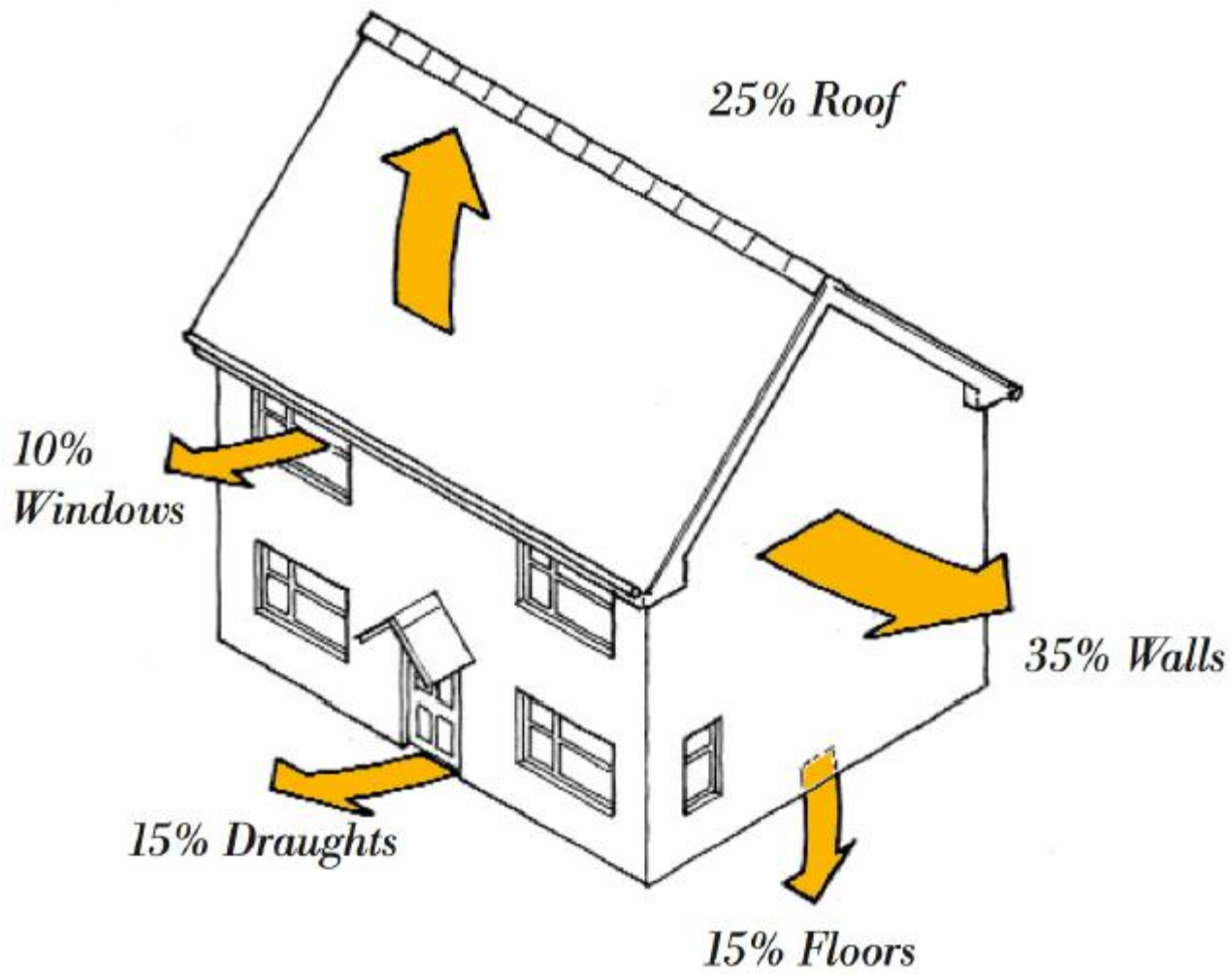


Potential and limitations of infrared thermography on unventilated walls

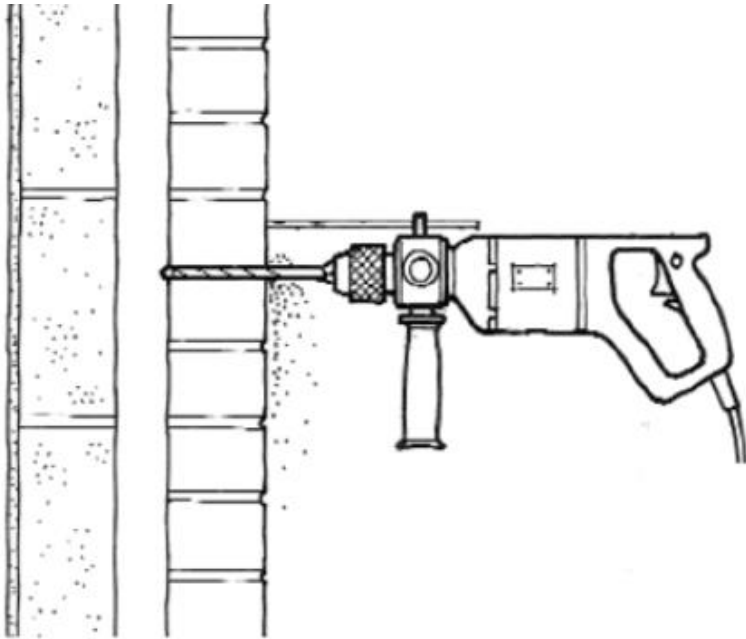
Katrien Maroy

Nathan Van Den Bossche, PhD

Marijke Steeman, PhD

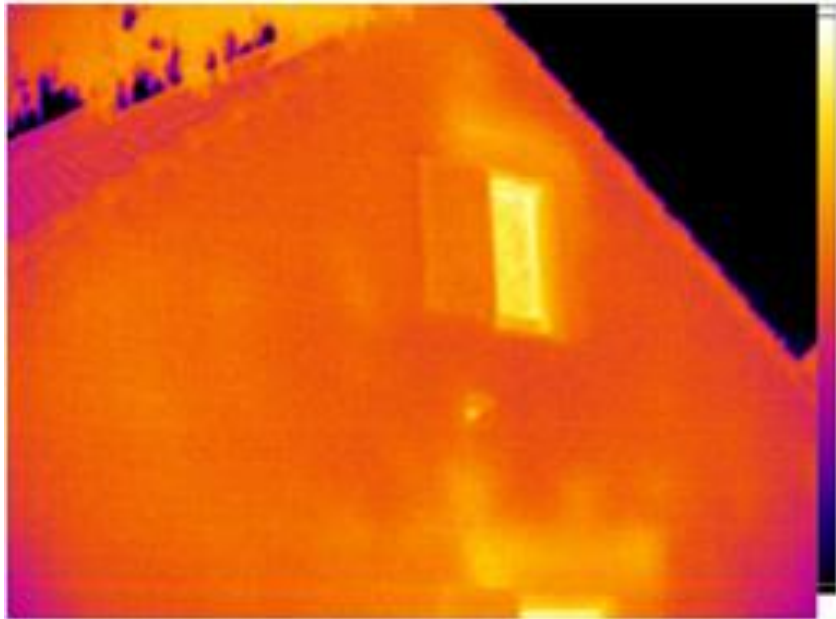


Solution?



75% of all renovation projects

Practice?

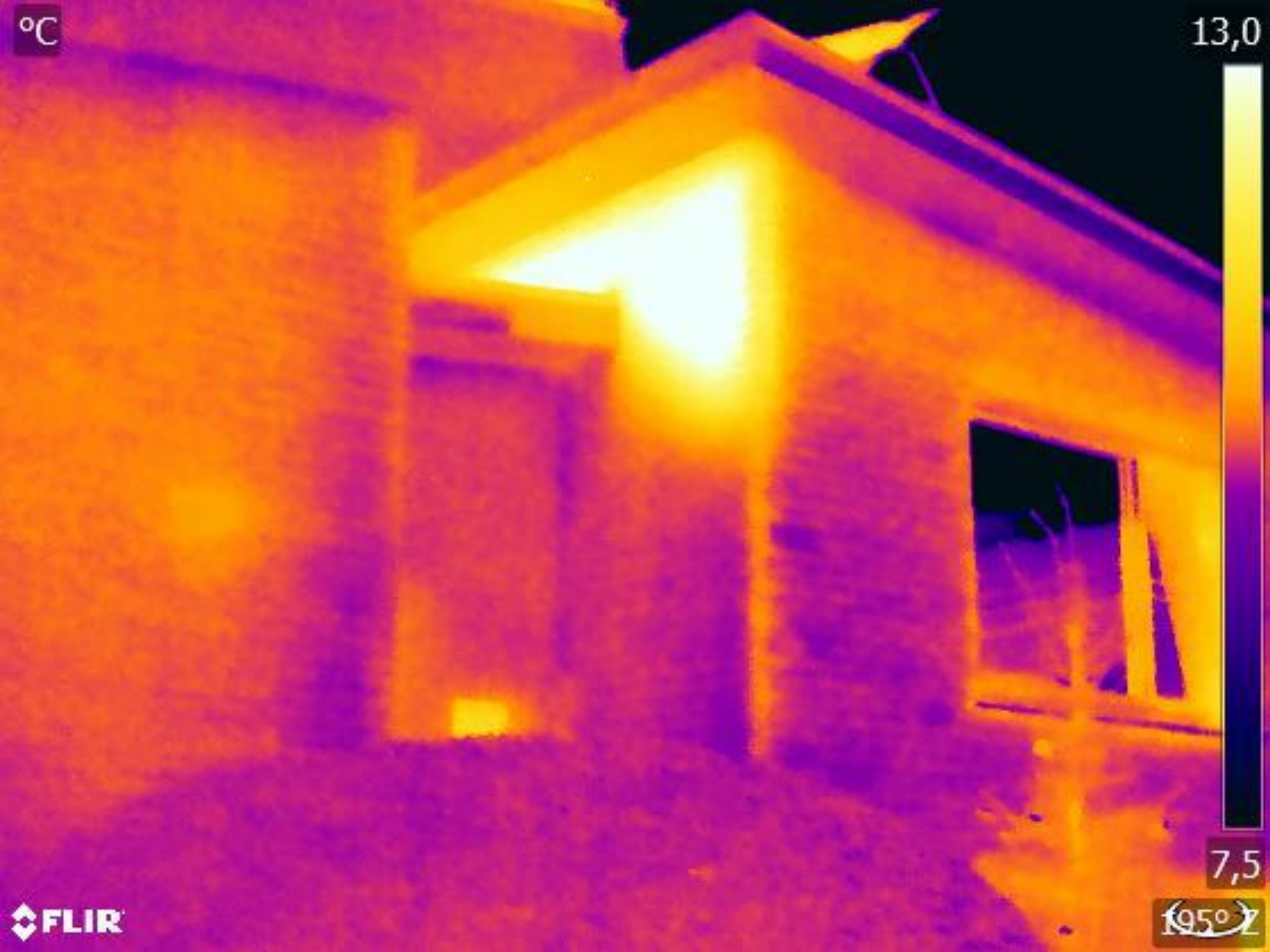


Inspection tools

- Destruction
- Endoscopy
- Thermography?

°C

13,0



7,5

195°

FLIR



Overview

The accuracy of thermography

Emissivity and reflected temperature

Camera use

Boundary conditions

Infrared inspection of cavity filling

Dynamic simulations

Case studies

Overview

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Camera use

Boundary conditions

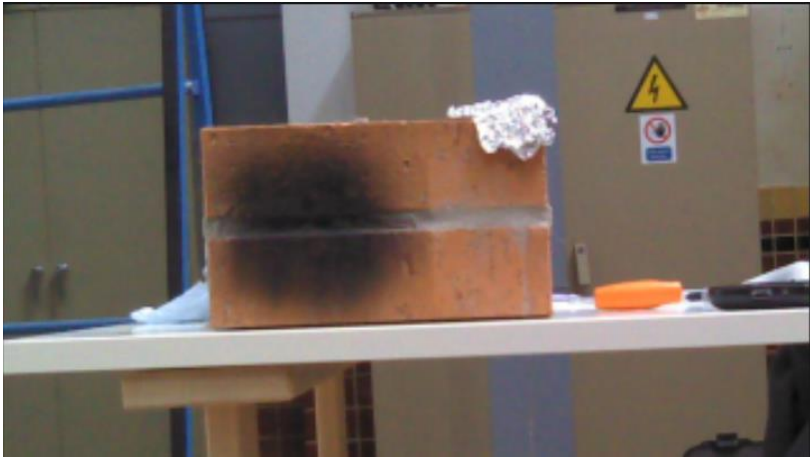
Infrared inspection of cavity filling

Dynamic simulations

Case studies

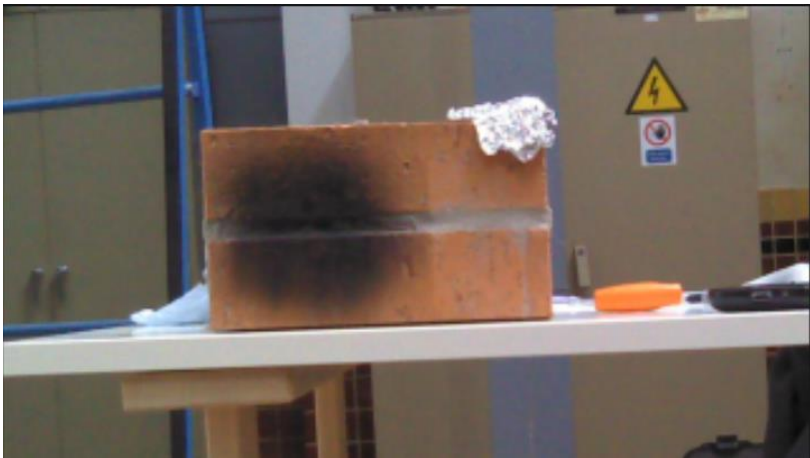
Emissivity and Reflected temperature

$$W_{tot} = \varepsilon \cdot W_{obj} + \rho \cdot W_{amb} + (1 - \tau_{atm}) \cdot W_{atm} \quad [\text{W/m}^2]$$



Emissivity and Reflected temperature

$$W_{tot} = \varepsilon \cdot W_{obj} + \rho \cdot W_{amb} + \underbrace{(1 - \tau_{atm}) \cdot W_{atm}}_{\substack{\tau_{atm} = 1 \text{ in} \\ \lambda = 3-5 \mu\text{m and } 8-14 \mu\text{m}}} \quad [\text{W/m}^2]$$

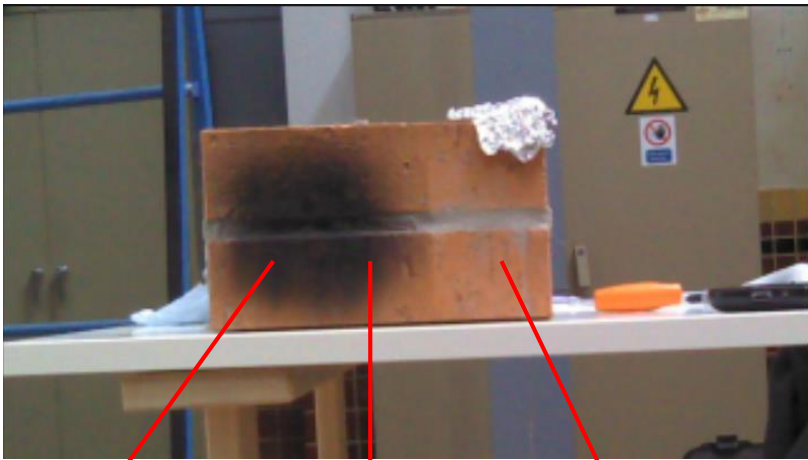


$\tau_{atm} = 1$ in
 $\lambda = 3-5 \mu\text{m}$ and $8-14 \mu\text{m}$

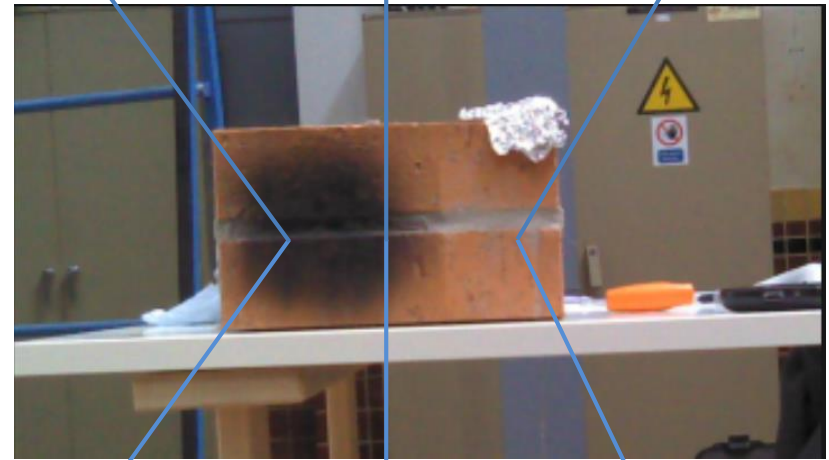
→ Spectrum of IR-camera

Emissivity and Reflected temperature

$$W_{tot} = \varepsilon \cdot W_{obj} + \rho \cdot W_{amb}$$



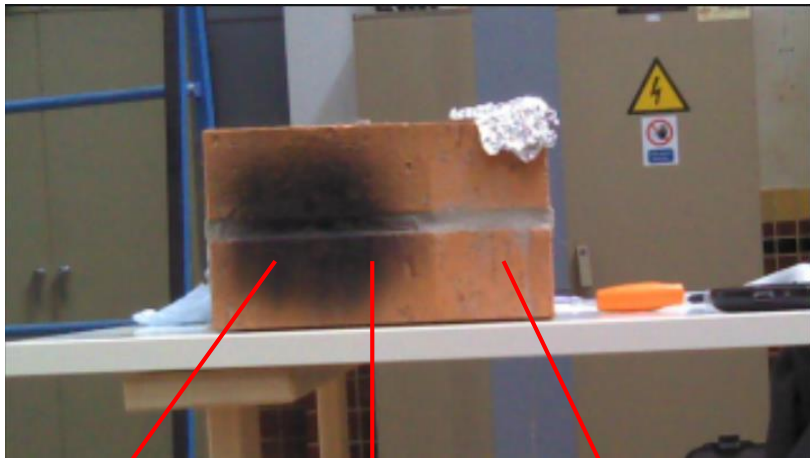
Emissivity ε



Reflection $\rho = 1 - \varepsilon$

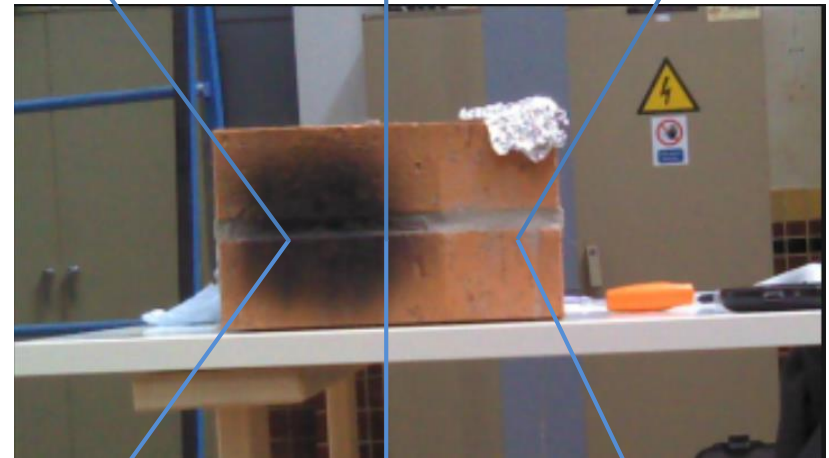
Emissivity and Reflected temperature

Example: Brick $\rightarrow \varepsilon = 0,90$



Emissivity ε

$$W_{tot} \sim 90\% \theta_{obj}$$



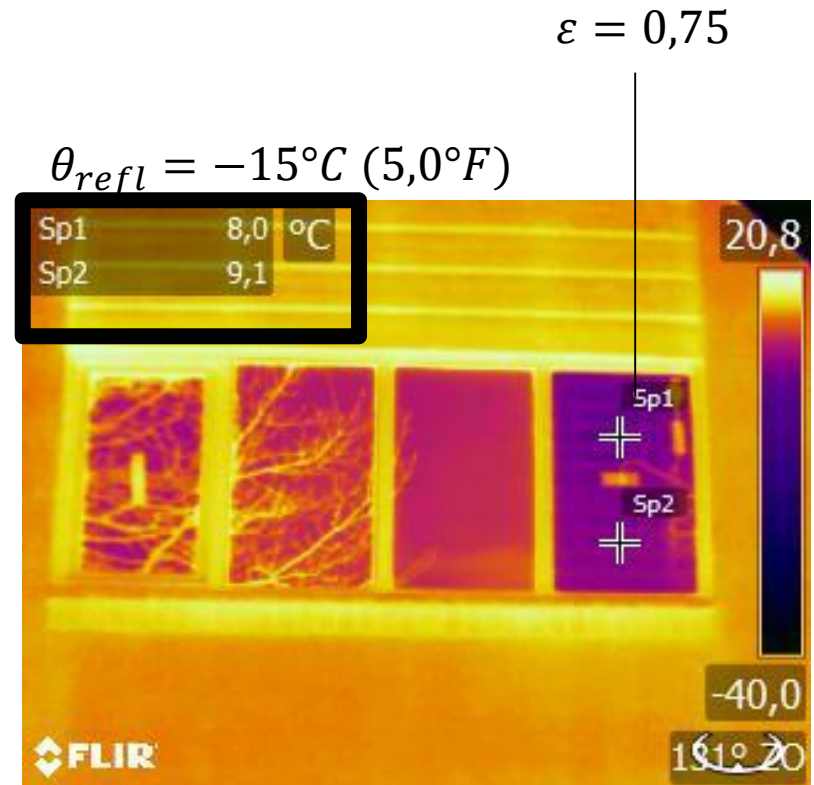
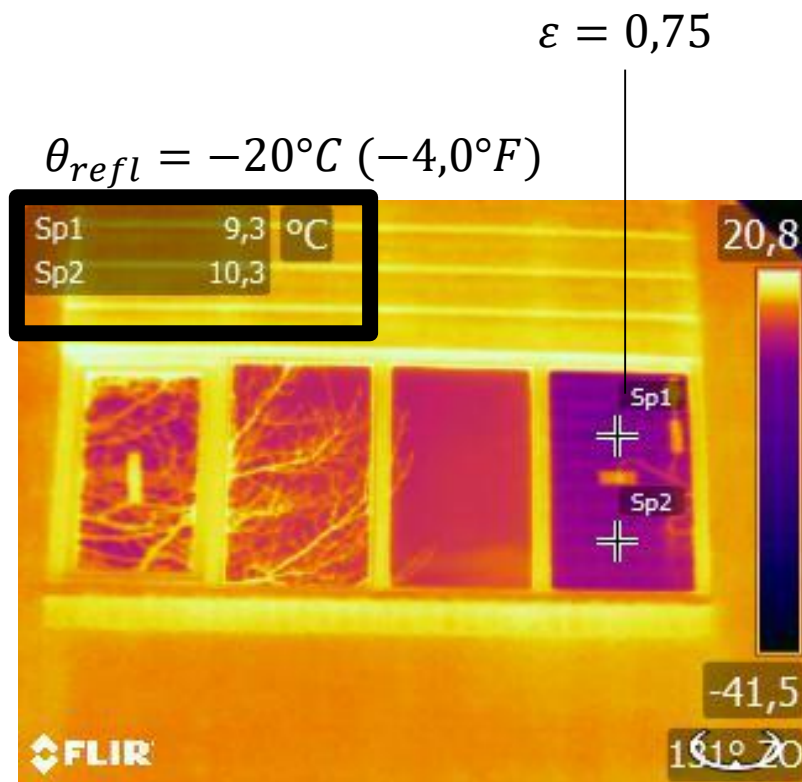
Reflection $\rho = 1 - \varepsilon$

$$W_{tot} \sim 10\% \theta_{refl}$$

Emissivity and Reflected temperature

Use correct values!

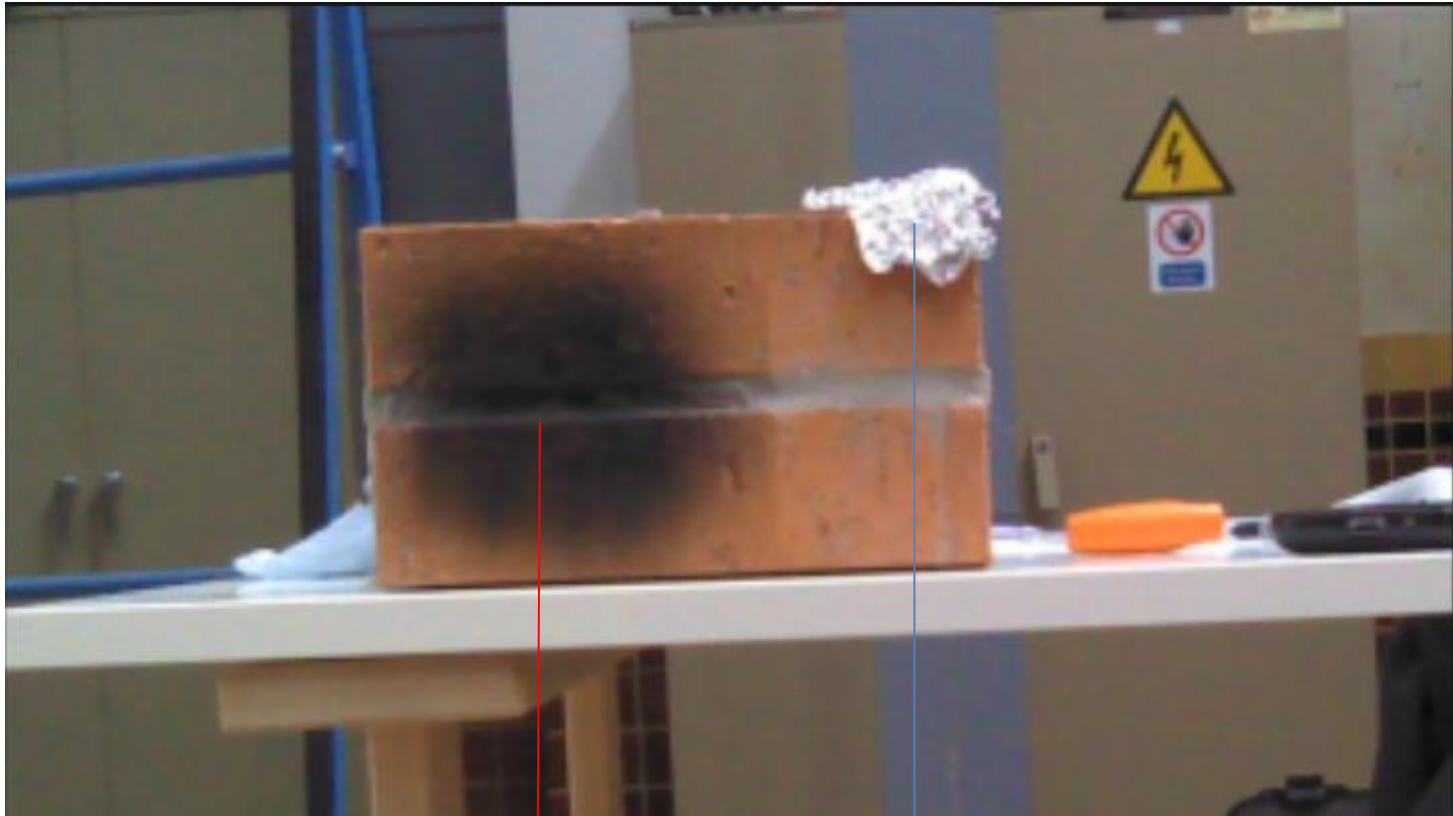
Example: measurements in clear sky



Accuracy difference : $1,2^{\circ}\text{C} (2,16^{\circ}\text{F})$

Emissivity and Reflected temperature

In-situ determination



Determine ϵ
ASTM E1993-99a

Determine θ_{refl}
ASTM C1060-11a

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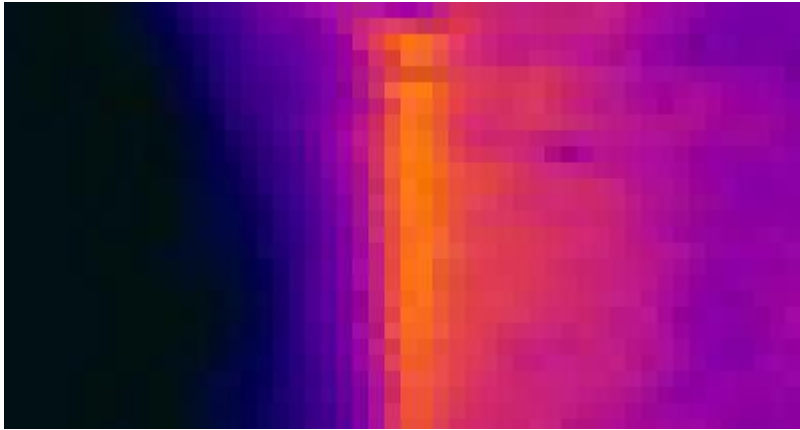
Boundary conditions

Infrared inspection of cavity filling

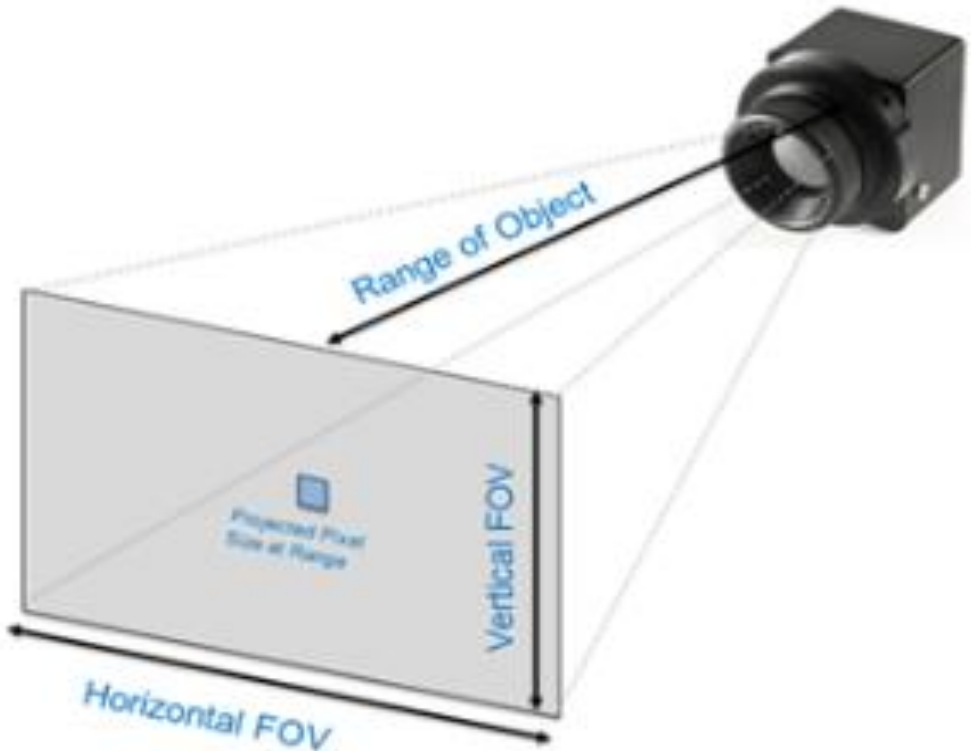
Dynamic simulations

Case studies

Camera use



Camera use



Camera use



Camera use

Different FOV's of the lens

$\theta_s = 20,0^\circ\text{C} (68,0^\circ\text{F})$



45°x33,8°

$\theta_s = 19,4^\circ\text{C} (67,3^\circ\text{F})$



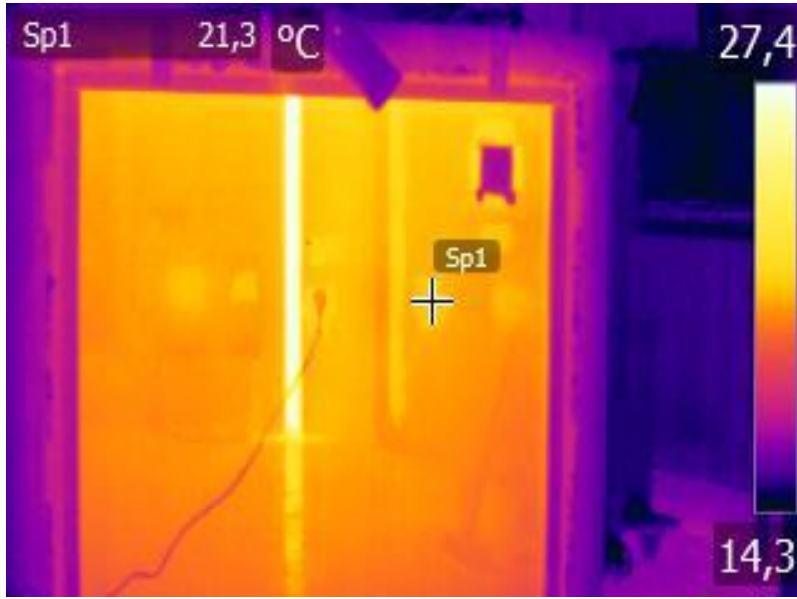
25°x19°

Camera use

Resolution



640 X 480



320 X 240

Camera use

Standard deviation: $\pm 2^{\circ}\text{C}$ (3,6 $^{\circ}\text{F}$)

Noise Equivalent Temperature Difference (NETD)

Imaging Specifications

FEATURES	FLIR E40	FLIR E50	FLIR E60
Temperature range	-4 to 1202°F (-20 to 650°C)	-4 to 1202°F (-20 to 650°C)	-4 to 1202°F (-20 to 650°C)
Thermal sensitivity (N.E.T.D)	<0.07°C at 30°C	<0.05°C at 30°C	<0.05°C at 30°C
Detector type - Focal plane array; (FPA) uncooled microbolometer	160 x 120 pixels	240 x 180 pixels	320 x 240 pixels
MSX® Thermal Image Enhancement	Yes	Yes	Yes
Picture-in-Picture (P-i-P)	Fixed P-i-P	Scalable P-i-P	Scalable P-i-P
MPEG 4 Video Recording	Yes	Yes	Yes
Video Camera w/Lamp & Laser	3.1MP/LED Lamp/Laser pointer	3.1MP/LED Lamp/Laser pointer	3.1MP/LED Lamp/Laser pointer
Digital Zoom	2X Continuous	4X Continuous	4X Continuous
Image annotation	Voice (60s)/Text Comments	Voice (60s)/Text Comments	Voice (60s)/Text Comments
Moveable Spot	3 Spotmeters	3 Spotmeters	3 Spotmeters
Area Box	3 Area Boxes (full image with min/max/avg)	3 Area Boxes (full image with min/max/avg)	3 Area Boxes (full image with min/max/avg)
Delta T	Yes	Yes	Yes
Data Communication Interface	USB-mini, USB-A, Composite Video, Bluetooth, Wi-Fi	USB-mini, USB-A, Composite Video, Bluetooth, Wi-Fi	USB-mini, USB-A, Composite Video, Bluetooth, Wi-Fi

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$\theta_i - \theta_e$

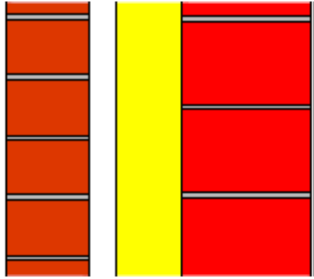
> 10°C (18 °F)

Weather conditions

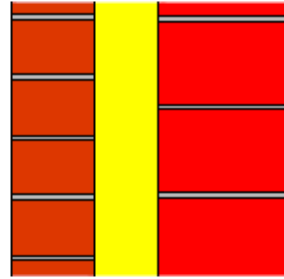
No sun, no clear sky, no wind

→ How long does the influence remain?

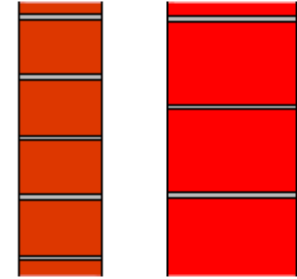
Boundary conditions



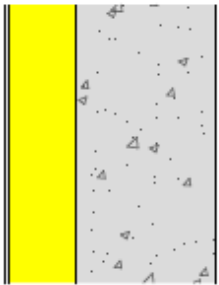
$$U = 0,22 \text{ W/m}^2\text{K}$$
$$E = 531,21 \text{ J/m}^2\text{KVs}$$



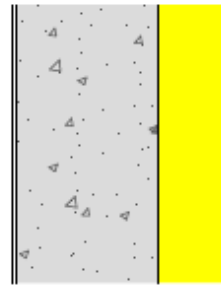
$$U = 0,22 \text{ W/m}^2\text{K}$$
$$E = 531,21 \text{ J/m}^2\text{KVs}$$



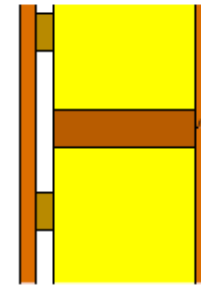
$$U = 1,00 \text{ W/m}^2\text{K}$$
$$E = 531,21 \text{ J/m}^2\text{KVs}$$



$$U = 0,22 \text{ W/m}^2\text{K}$$
$$E = 32,40 \text{ J/m}^2\text{KVs}$$

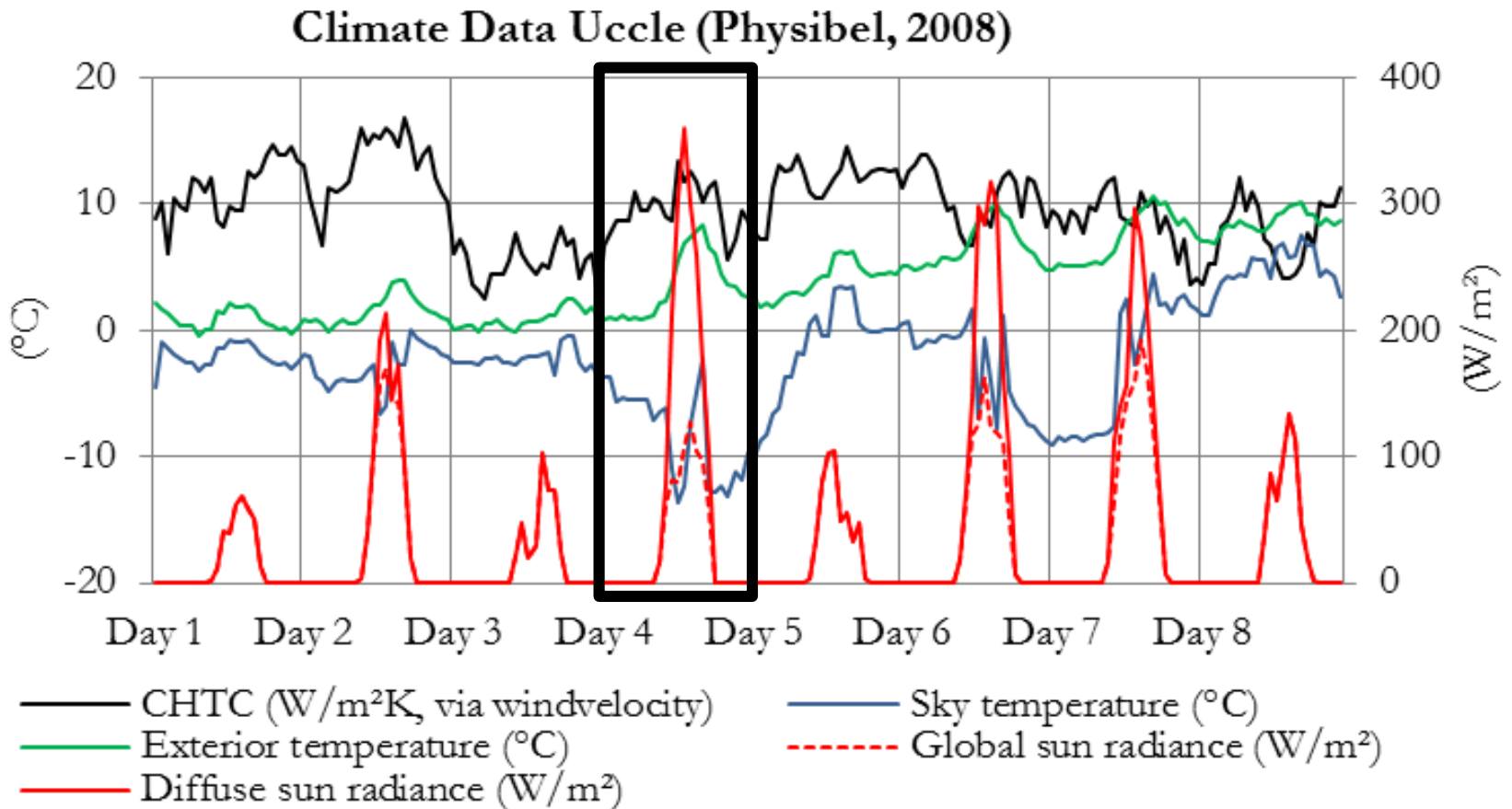


$$U = 0,22 \text{ W/m}^2\text{K}$$
$$E = 2500 \text{ J/m}^2\text{KVs}$$



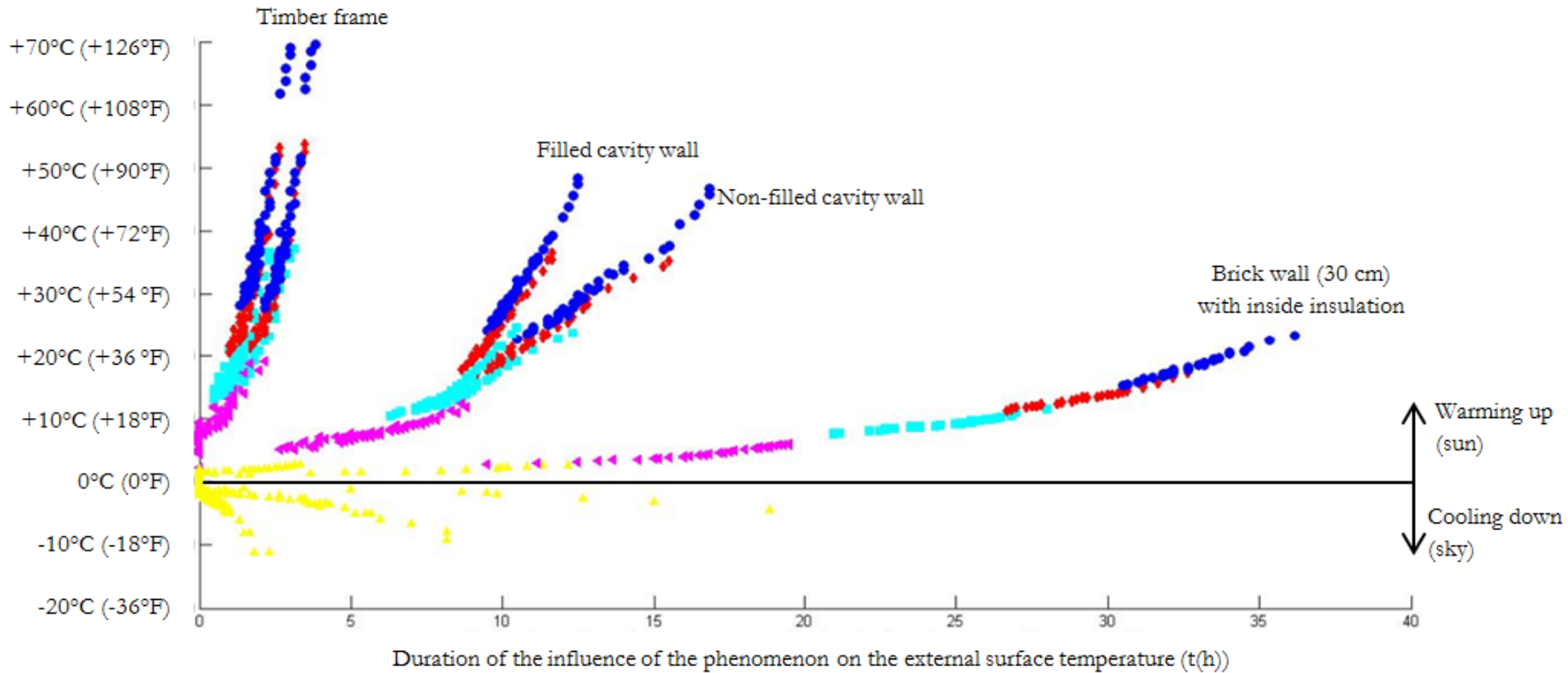
$$U = 0,22 \text{ W/m}^2\text{K}$$
$$E = 32,40 \text{ J/m}^2\text{KVs}$$

Boundary conditions

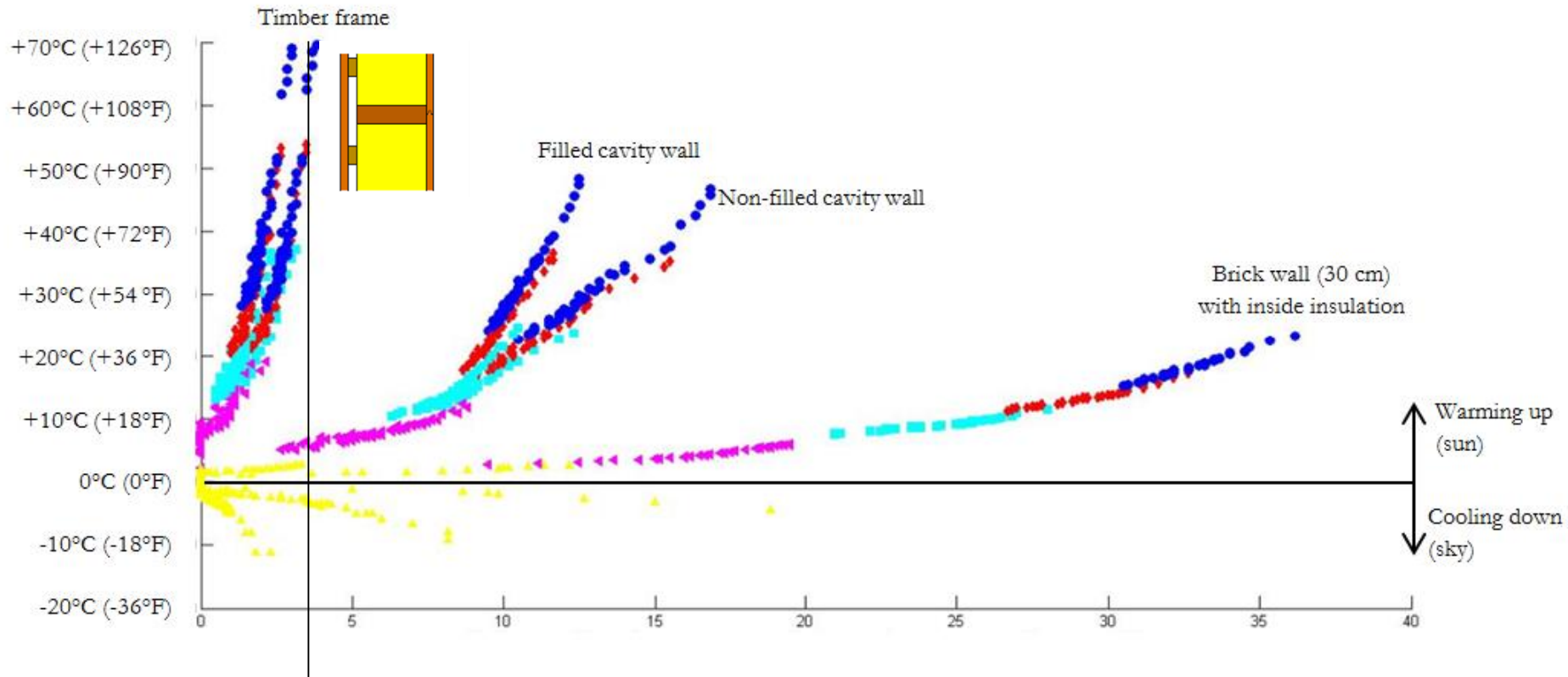


Boundary conditions

Maximum external surface temperature difference with respect to the steady state condition



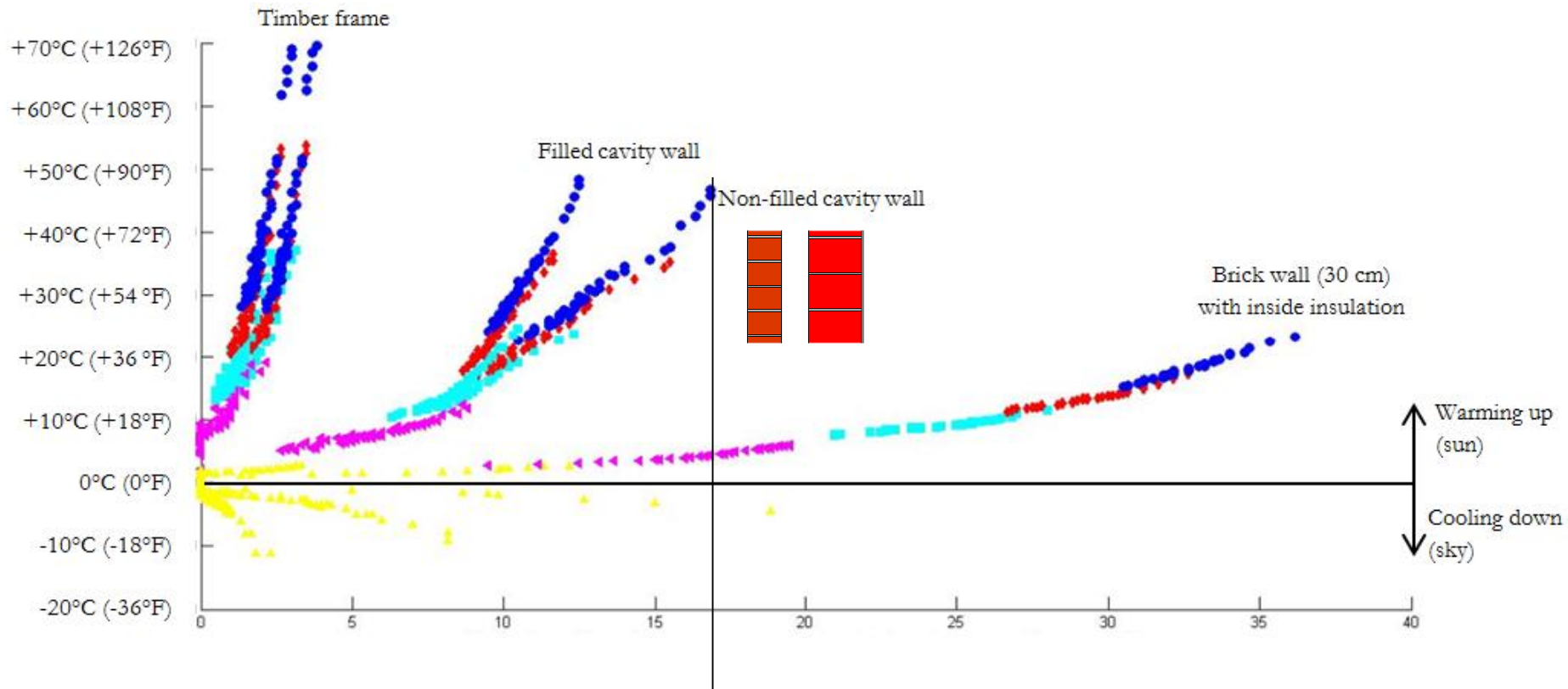
Boundary conditions



4 hours waiting
in heavy clouded
windless weather

(Van De Vijver, 2014)

Boundary conditions



17 hours waiting
in heavy clouded
windless weather

(Van De Vijver, 2014)

Overview

The accuracy of thermography

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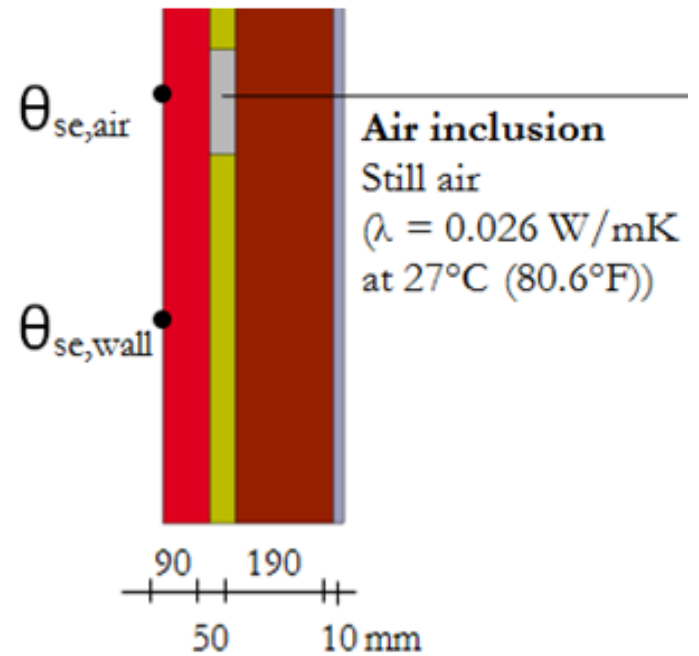
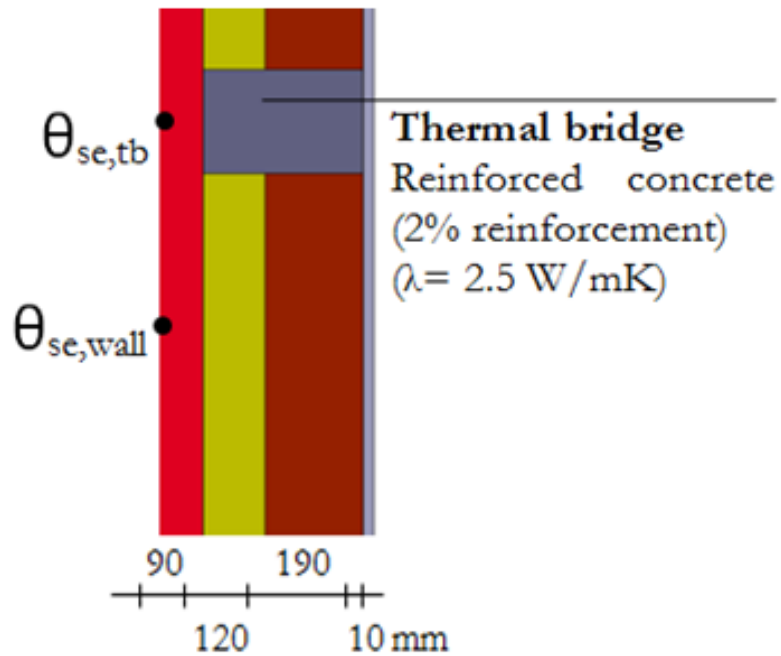
Boundary conditions

Infrared inspection of cavity filling

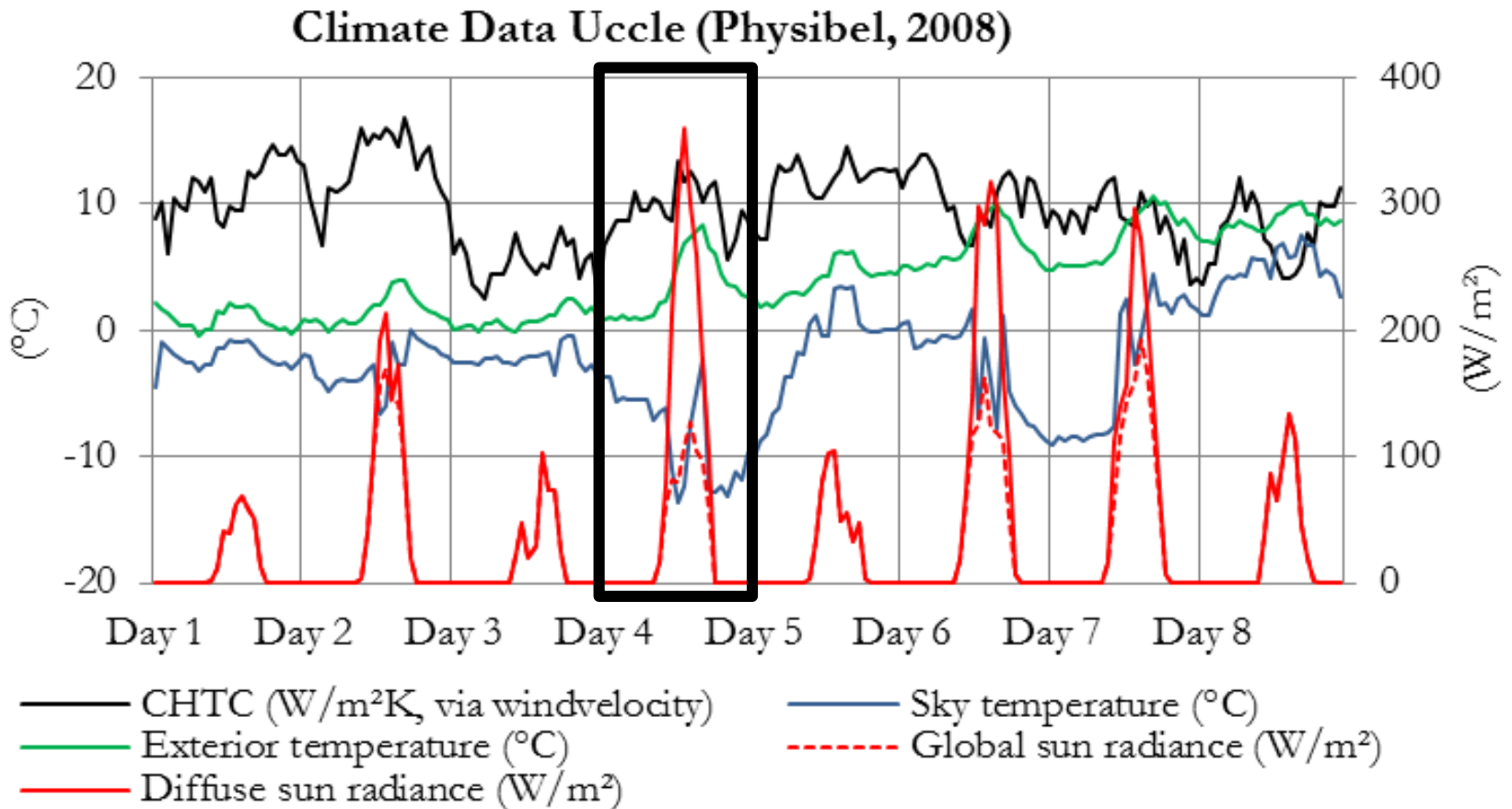
Dynamic simulations

Case studies

Dynamic simulations

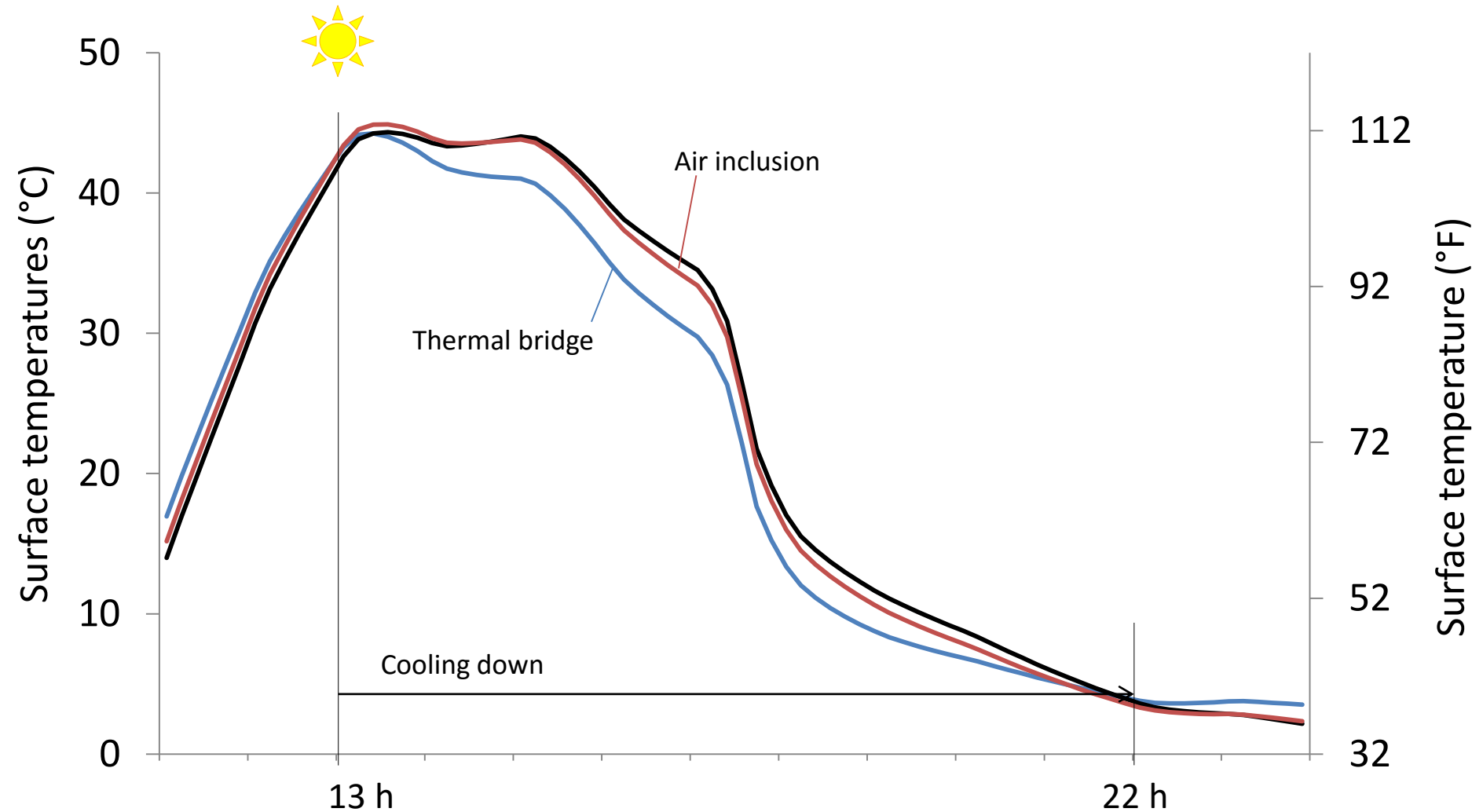


Dynamic simulations



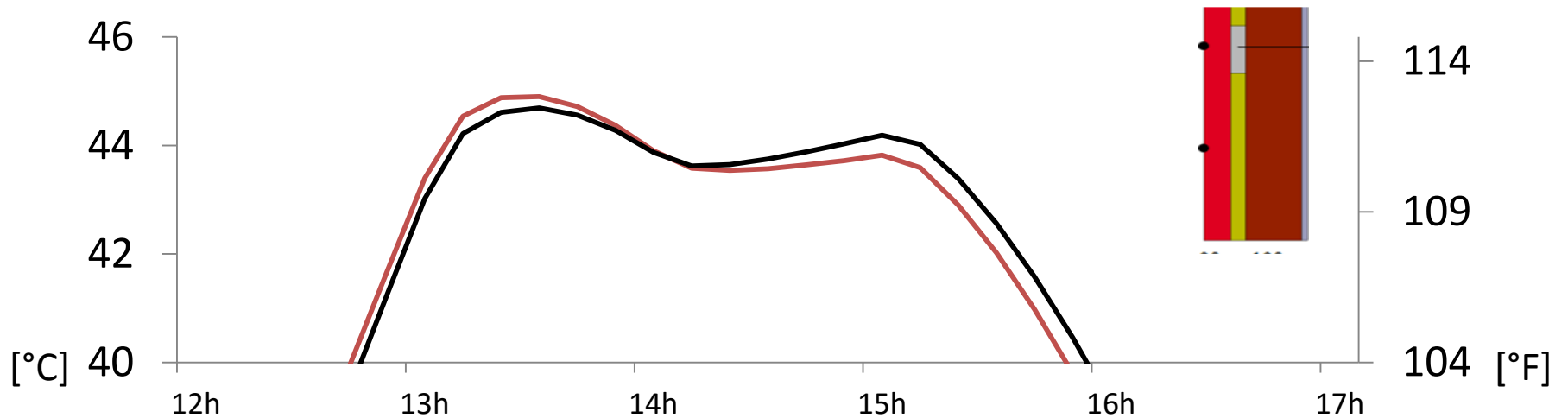
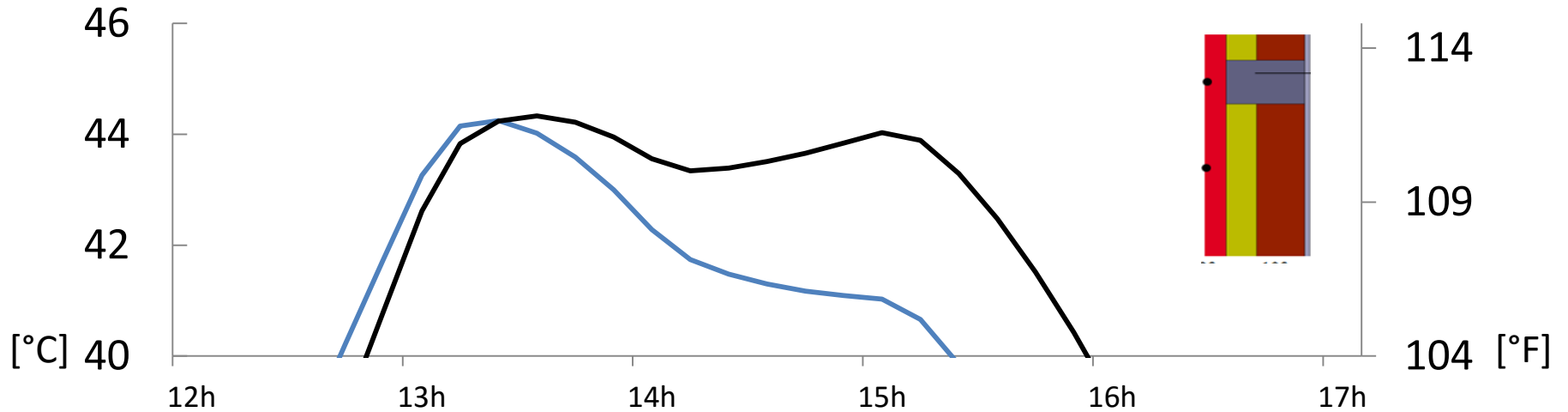
Dynamic simulations

Maximal sun radiation, Clear sky, No wind



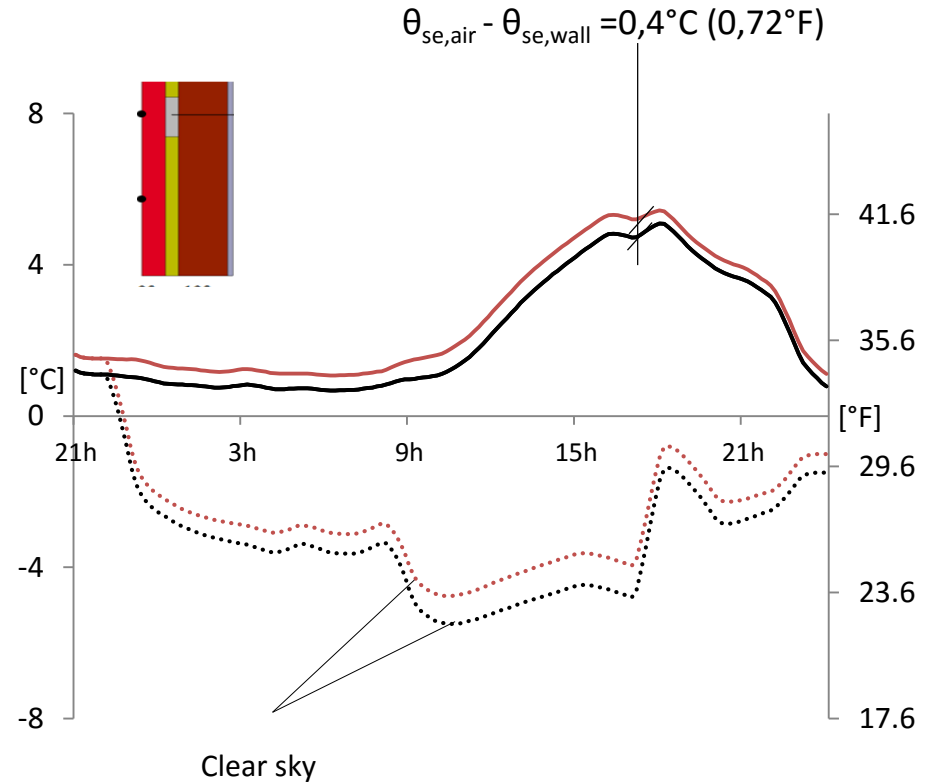
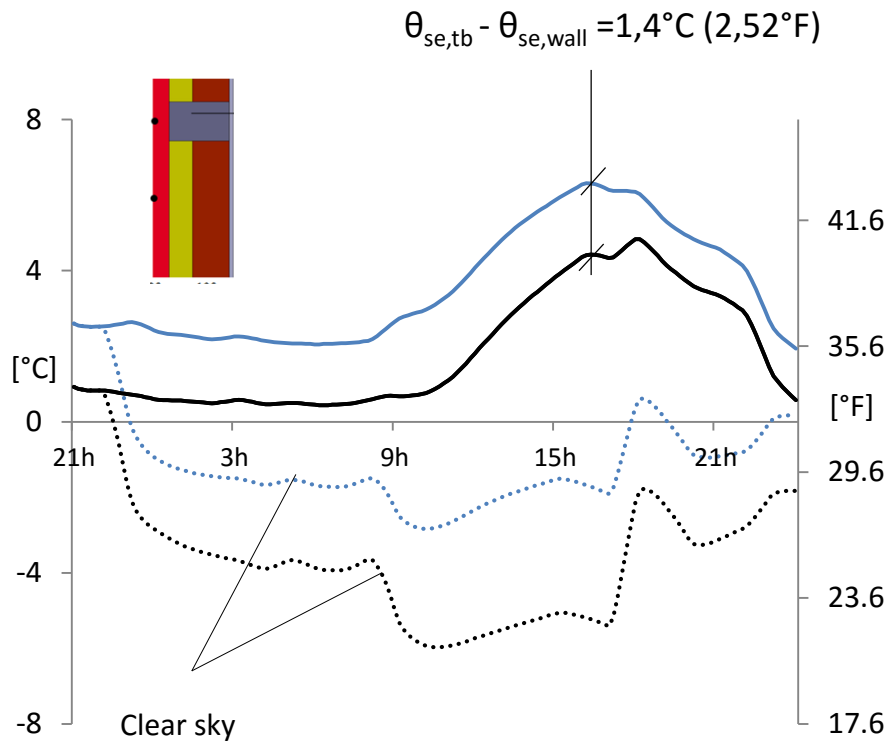
Dynamic simulations

Maximal sun radiation, Clear sky, No wind



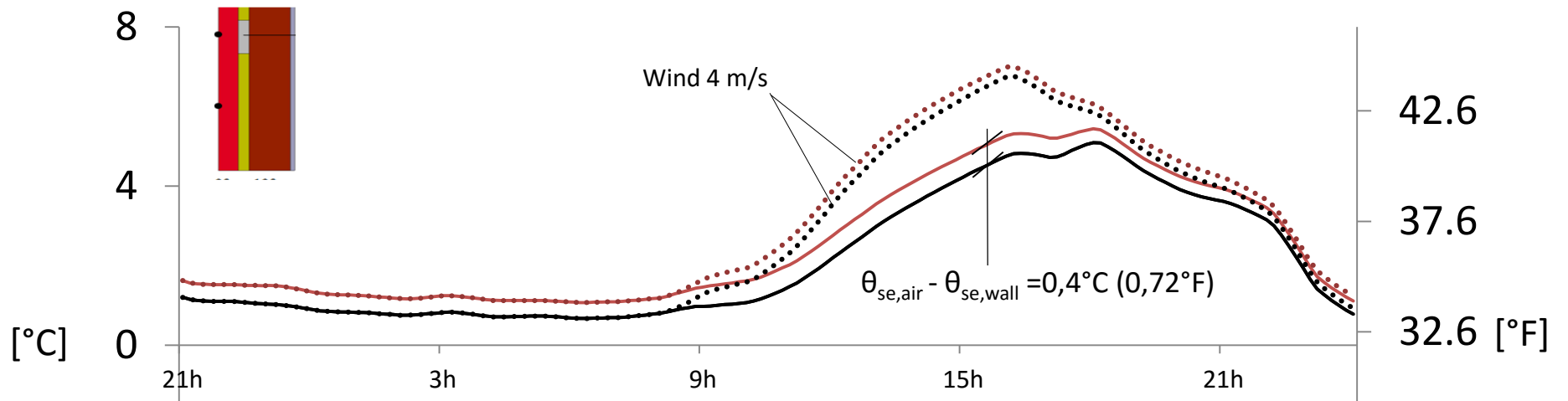
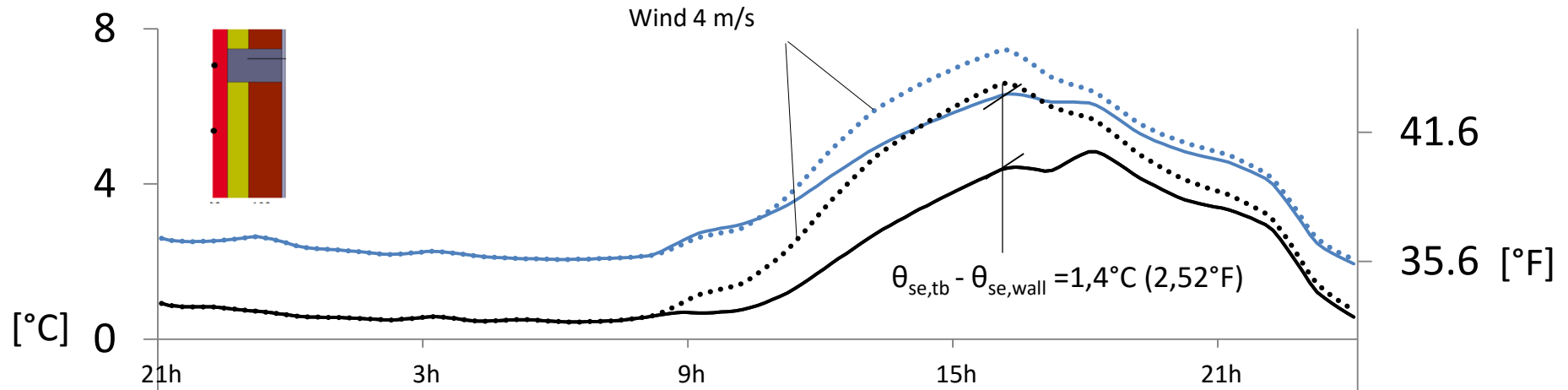
Dynamic simulations

No sun, **Clear sky vs. fully clouded**, No wind



Dynamic simulations

No sun, Fully clouded and **Wind (4 m/s) vs. No Wind**



Dynamic simulations

Only waiting times after sun radiation necessary

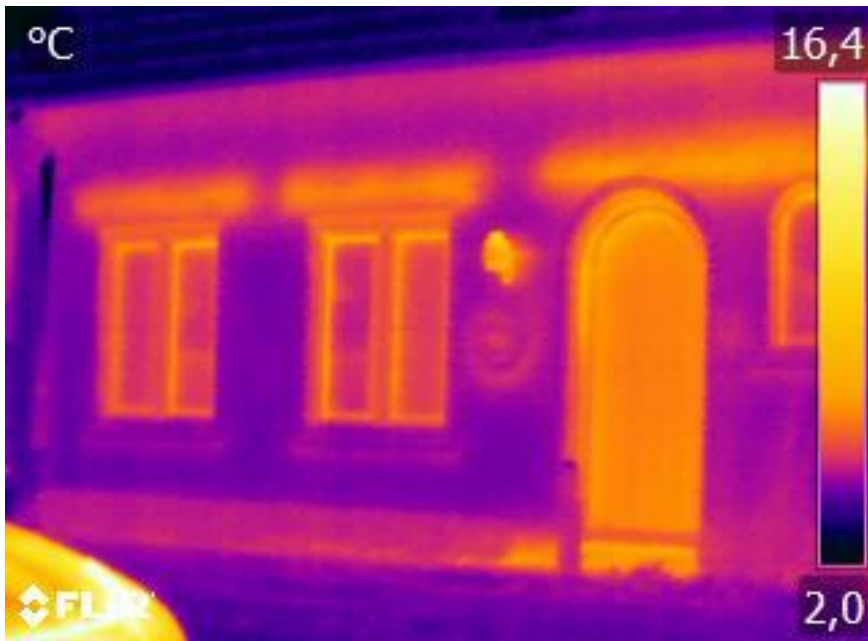
	Timber frame	Filled cavity wall	Non-filled cavity wall	Partially filled cavity wall
11400 kJ/m ²	0 – 1,5h	3,5 – 7h	2 – 6,5h	3,5 – 7h
8400 kJ/m ²	0 – 1h	2 – 6h	0,2 – 5h	2 – 6h
5600 kJ/m ²	0h	0 – 4,5h	0 – 3,5h	0 – 4,5h
2750 kJ/m ²	0h	0 – 2h	0 – 0,5h	0 – 2h
0 kJ/m ²	0 – 0,2h	0 – 1h	0 – 0,2h	0 – 1h

+ Temperature difference > 10°C (18°F) across the wall

Dynamic simulations

In practice:

Go measure in wintertime, before sunrise



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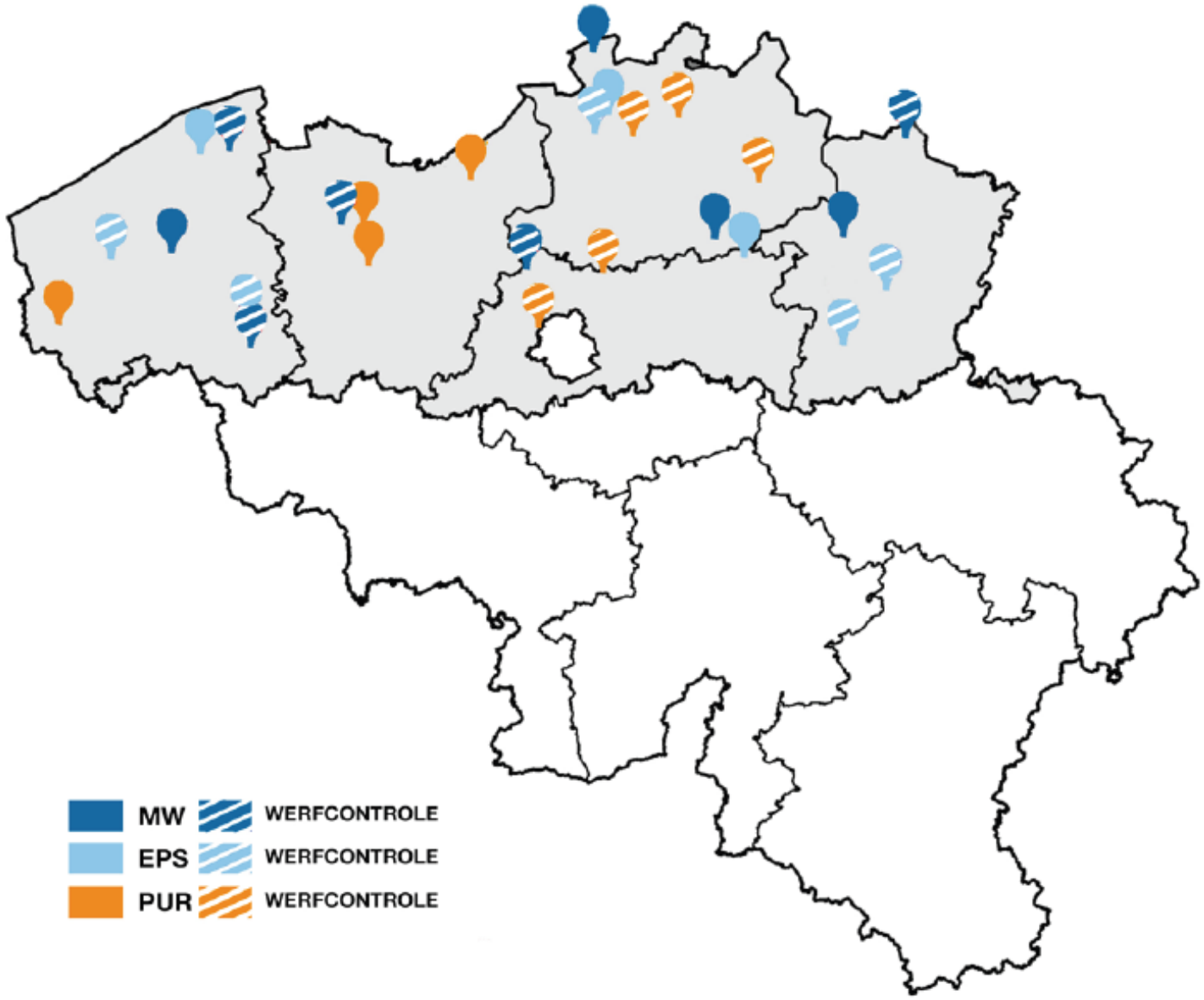
Boundary conditions

Infrared inspection of cavity filling

Dynamic simulations

Case studies

Case studies



(Beulque, 2014)

Case studies

Common flaws

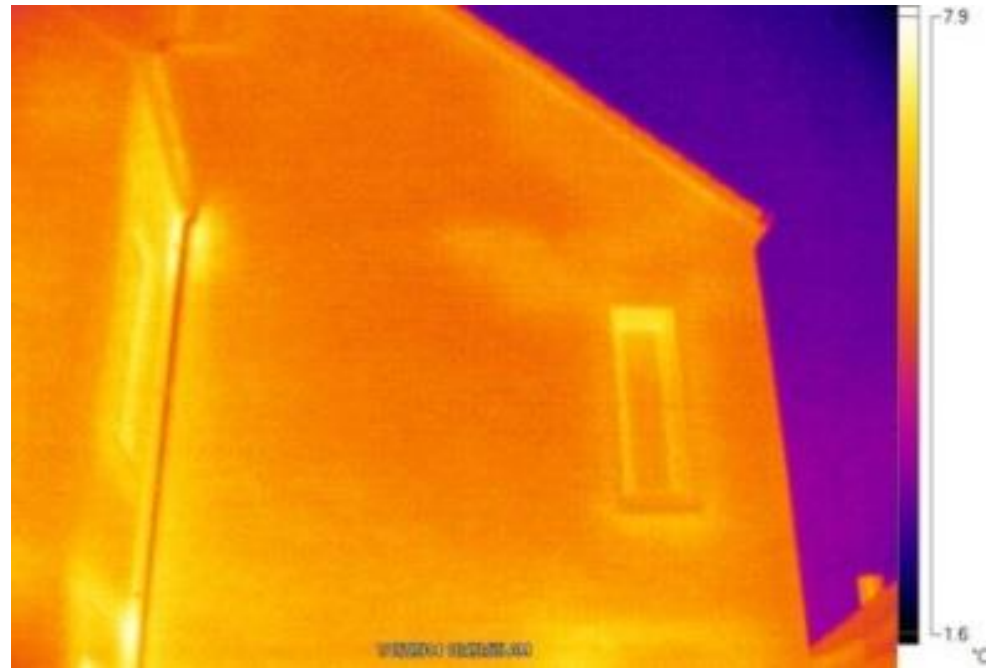
- Poor or lacking measurement data of the cavity width
- Ignorance towards the minimum cavity width (< 5 cm or 1,96")
- Insufficient number of bore holes
- Incorrect glue flow rate of the EPS pearls
- Incomplete filling at corners and cavity interruptions
- Missing bore holes due to vegetation or cables
- Open parpens at the top
- Parpens and openings in the inner cavity leaf during cavity filling



Which of these flaws are detectable with thermography?

Case studies

Know what you can expect → Execution report



Vegetation during cavity filling work
→ no bore holes
→ insufficient filling locally

Case studies

Know what you can expect → Execution report



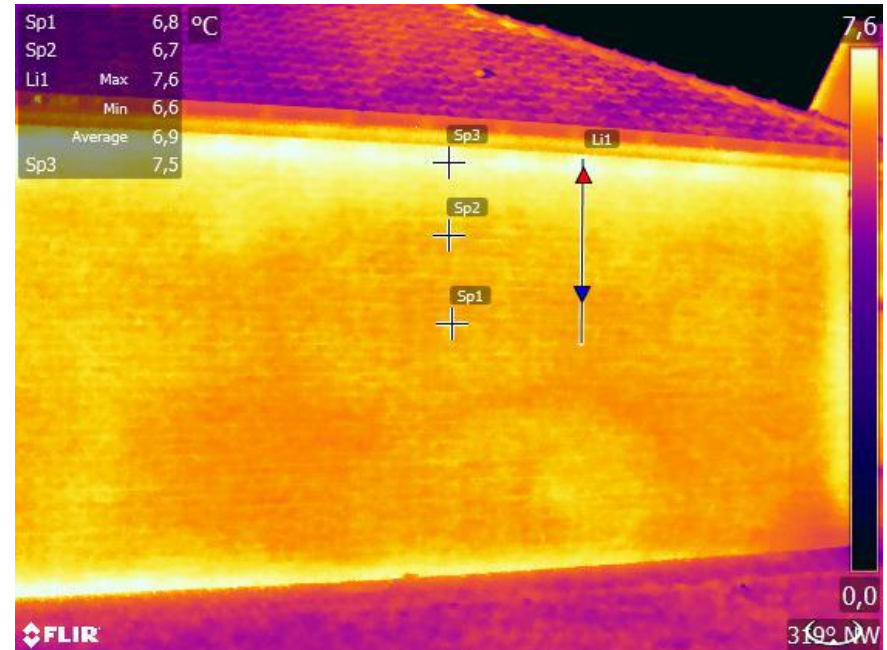
Filling with EPS-pearls
Glue stacked at the corners

Case studies

Know what you can expect → Execution report



Chimney effect?



EPS pearls escaped through openings in the inner cavity wall

$$U_{\text{measured}} = 0,476 \text{ W/m}^2\text{K (+26\%)}$$

$$U_{\text{calc}} = 0,377 \text{ W/m}^2\text{K}$$

Conclusion

Yes, thermography has potential

General overview

Thermal bridges are clearly visible

- Avoid sun and $\theta_i - \theta_e > 10^\circ\text{C}$ (18°F)
- Predictable locations and shape (above windows, at floors,...)

However, do not draw direct conclusions

The ease by which thermal deficiencies are recognized depends on:

Type, shape, geometry of the building, condition of the surface, location of the pattern, prior weather conditions.....

Conclusion

Yes, thermography has potential

General overview

Thermal bridges are clearly visible

- Avoid sun and $\theta_i - \theta_e > 10^\circ\text{C}$ (18°F)
- Predictable locations and shape (above windows, at floors,...)

To indicate the location for further research with

- An endoscopy
- Destructive research

Potential and limitations of infrared thermography on unventilated walls

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