# DEVELOPMENT OF COOLING DEGREE-HOUR WEATHER DATA FOR ASHRAE STANDARD 90.2-1993 

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#### Abstract

ASHRAE Standard 90.2-1993, "Energy-Efficient Design of New Low-Rise Residential Buildings," uses cooling degreehours to base $74^{\circ} \mathrm{F}(\mathrm{CDH74)}$ as a cooling weather variable. Because CDH74 was not readily available or published, it was developed for application with the standard. The basis for the development was a statistical autocorrelation technique derived by analyzing hourly data for a complete year from 101 locations. These 101 locations were weather stations in the United States. They accounted for almost all cooling climatic conditions in North America. They did not account for the most severe heating climatic conditions in North America, where the cooling impact is minimal. The theoretical development of the autocorrelation technique, the resulting terms derived from the analysis, and the extrapolation of those terms to extreme heating climatic locations are presented. Application of the procedure only requires knowledge of the monthly average dry-bulb temperature and the monthly average dry-bulb temperature standard deviation. This information is published by the National Oceanic and Atmospheric Administration in the United States and by the Atmospheric Environment Service in Canada. After the methodology was developed, it was used to create CDH74 for 3,349 locations in the United States and 1,847 locations in Canada. The resulting tables were published in the standard.


## INTRODUCTION

ASHRAE Standard Project Committee (SPC) 90.2 was responsible for the development of ASHRAE Standard 90.2-1993, "Energy-Efficient Design of New Low-Rise Residential Buildings" (ASHRAE 1993). The SPC started the development by using the Departmetn of Engergy (DOE)-2.1A hourly simulation program to accurately predict the heating and cooling season envelope loads in multiple locations for each envelope component, including ceilings, walls, doors, and fenestration (LBL 1981). Heating and cooling season loads for foundations (basements, crawlspaces, and slabs) were developed using a two-dimensional finite-difference procedure with hourly weather data. All of these component loads were then used to develop a simplified heating and cooling load factor procedure that predicted envelope loads and evaluated trade-offs among envelope components (McBride et al. 1991). The load factors also were used in setting the envelope criteria (McBride 1991). The load factor procedure uses simple weather variables to correlate the heating and cooling season results of the hourly simulations. Heating results were correlated using heating degreedays to base $65^{\circ} \mathrm{F}$ (HDD65). Cooling results were correlated using cooling degree-hours to base $74^{\circ} \mathrm{F}$ (CDH74).

For the SPC development effort CDH74 was derived using hourly weather data tapes of test reference year
(TRY) (Stamper 1977; NOAA 1976), California thermal zones (CTZ) (CEC 1988), and weather year for energy calculations (WYEC) (Crow 1981). However, for application of the standard, a list more extensive than 101 locations was desired. Hourly recordings of temperatures are only recorded at the first-order weather stations represented by the hourly weather data tapes. To expand the number of locations in Standard 90.2 required using alternate data. Monthly average dry-bulb temperatures and standard deviations are available for 3,349 locations in the United States and 1,847 locations in Canada. These data routinely are used to calculate heating and cooling degree-days to various base temperatures and were selected for development of CDH74.

## BACKGROUND

Methods to calculate heating and cooling degreedays to any base temperature have been well established using monthly average dry-bulb temperatures and standard deviations (Thom 1952, 1954a, 1954b, 1954c). Typically, the monthly average temperatures and standard deviations are based on a 30 -year period of record to ensure they are representative.

The first attempt in calculating CDH 74 was to simply assume the dry-bulb temperatures within a month were uncorrelated and normally distributed. Then the

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CDH74 Predicled Using Cooling Degree Days Times 24


Figure I Comparisons of CDH74 calculated from CDD vs. hourly weather data fapes.
distribution was appropriately integrated and multiplied by 24 hours times the number of days to yield the monthly cooling degree-days. This procedure consistently underpredicted CDH74 for all 101 locations (Figure 1).

Failure of this simple approach led to discussions with Dr. Nathaniel B. Guttman (Guttman 1990). He suggested that estimates of the monthly standard deviations could be improved by accounting for the pairwise correlations among days. Further improvements would account for the autocorrelation of hourly dry-bulb temperatures. Autocorrelation is a measure of the time sequence dependence of successive values. It applies when successive values are not independent and random. Autocorrelation techniques are available that account for continuous variables such as hourly dry-bulb temperatures (Brooks and Carruthers 1953; Snedecor and Cochran 1967; Kenney 1939).

Currently, there is no universally accepted method available to calculate cooling degree-hours using monthly average dry-bulb temperatures and monthly average standard deviations.

## OBJECTIVE

The objective of this research was to develop a procedure to calculate CDH 74 using monthly average dry-bulb temperatures and monthly average standard deviations
reported by NOAA (1951-1980) and AES (1951-1980) for 30 -year periods of record.

## TECHNICAL APPROACH

Multiple steps were required in developing a methodology to calculate CDH74. First, the specific autocorrelation coefficient for individual months and temperature intervals ( $r_{i, j}$ ) had to be determined from hourly tapes. Second, a statistically average autocorrelation coefficient by month and temperature interval $\left(r_{A V G i, j}\right)$ had to be determined. Third, $r_{A V G i, j}$ had to be tested against CDH74 from hourly weather data tapes. Fourth, $r_{A V G i, j}$ had to be extrapolated to account for all climates in the United States and Canada. Finally, $r_{A V G i, j}$ was used to calculate CDH74 for 3,349 locations in the United States and 1,847 locations in Canada. Each of these major steps will be presented.

## Determination of Specific Autocorrelation Coefficients by Month and Temperature Interval

In equation form, the autocorrelation coefficient for the $i^{\text {th }}$ month and the $j^{\text {th }}$ temperature interval is

$$
\begin{equation*}
r_{i, j}=\frac{N H_{i} \cdot\left(\sigma_{N, i} / \sigma_{T, i}\right)^{2}-1}{N H_{i}-1} \tag{1}
\end{equation*}
$$

where
$r_{i, j}=$ autocorrelation coefficient for the $i^{\text {th }}$ month and the $j^{\text {th }}$ temperature interval (dimensionless),
$i=$ month,
$j=$ temperature interval $\left(10^{\circ} \mathrm{F}\right)$,
$N H_{i}=$ number of hours in $i^{\text {th }}$ month (h),
$\sigma_{N, i}=$ standard deviation of monthly average temperatures for the $i^{i \text { th }}$ month $\left({ }^{\circ} \mathrm{F}\right)$ (derived from longterm data), and
$\sigma_{T, i}=$ standard deviation of temperatures within the $i^{\text {th }}$ month $\left({ }^{\circ} \mathrm{F}\right)$ (derived from hourly tapes).

Autocorrelation coefficients were determined for each month and the corresponding temperature interval from 101 hourly tapes using Equation 1. The locations and sources of the hourly tapes are presented in Table 1. There were 66 TRY, 16 CTZ , and 19 WYEC for a total of 1,212 months of hourly data. This was considered representative of U.S. and Canadian climates.

## Average Autocorrelation Coefficients

The 1,212 individual monthly results were then statistically analyzed to determine the average autocorrelation coefficient for each month in $10^{\circ} \mathrm{F}$ temperature intervals. The statistical results are presented in Table 2, which contains the number of months available (NO.), the average autocorrelation coefficient by month and temperature interval ( $r_{A V G i, j}$ ), and the standard deviation by month and temperature interval ( $r_{S D i, j}$ ) of the autocorrelation coefficient.

TABLE 1 Hourly Weather Locations

| TRY | CIZ | WYEC |
| :---: | :---: | :---: |
| 1 Albany, NY | 1 Arcata, CA | 1 Albuquerque. NM |
| 2 Albuquerque. NM | 2 Santa Rosa, CA | 2 Bismarck, ND |
| 3 Amarilo, IX | 3 Oakiond. CA | 3 Boise, ID |
| 4 Atlanto, GA | 4 Sunnyvale, CA | 4 Brownsville, IX |
| 5 Bangor ME | 5 Santa Maria, CA | 5 Chanteston, SC |
| 6 Bifminghom, AL | 6 Los Angeles, CA | 6 Clevelond, OH |
| 7 Bismarck, ND | 7 San Diego, CA | 7 Dayton, OH |
| 8 Botse, ID | 8 El Toro, CA | 8 El Paso, IX |
| 9 Boston, MA | 9 Posadeno. CA | 9 Fort Worth, TX |
| 10 Brownsville, TX | 10 San Bernadino, CA | 10 Lake Chorles, LA |
| 11 Buffalo, NY | 11 Red Bluff, CA | 11 Las Vegas, NV |
| 12 Burlington, VT | 12 Sacromento. CA | 12 Los Angeles, CA |
| 13 Charleston, SC | 13 Fresno, CA | 13 Modison, WI |
| 14 Charleston, W W | 14 Chino Lake, CA | 14 Medford, OR |
| 15 Cheyenne, WY | 15 Bythe, Ca | 15 Miamitl. |
| 16 Chicago, it | 16 Mount Shasto, CA | 16 Nashvile. IN 17 New York, NY 18 Seatle-Tacoma, WA 19 Tallohassee, FL |
| 17 Cincinnati, OH <br> 18 Cleveland, OH |  |  |
| 19 Cotumbla, MO |  |  |
| 20 Detroit, MI |  |  |
| 21 Dodge City, KS |  |  |
| 22 Duluth, MN |  |  |
| 23 El Poso, CA |  |  |
| 24 Fort Worth, TX |  |  |
| 25 Fresno. CA |  |  |
| 26 Great Falls, MT |  |  |
| 27 Houston, IX |  |  |
| 28 indianapolis, N |  |  |
| 29 Jackson, MS |  |  |
| 30 Jacksonvile. TN |  |  |
| 31 Kansas City, MO |  |  |
| 32 Loke Charles. LA |  |  |
| 33 Los Vegas. NV |  |  |
| 34 Little Rock, AR |  |  |
| 35 Los Angeles, CA |  |  |
| 36 Loulsville, KY |  |  |
| 37 Lubbock, IX |  |  |
| 38 Madison, WI |  |  |
| 39 Medford. OR |  |  |
| 40 Memphis , IN |  |  |
| 41 Mioml , FL |  |  |
| 42 Minneopolis, MN |  |  |
| 43 Noshville, IN |  |  |
| 44 New Orleans. LA |  |  |
| 45 New York, NY |  |  |
| 46 Norfolk, VA |  |  |
| 47 Okiohoma Cily, OX |  |  |
| 48 Omaho. NE |  |  |
| 49 Philodelphio, PA |  |  |
| 50 Phoenix, Az |  |  |
| 51 Pittsburgh, PA |  |  |
| 52 Portiond, ME |  |  |
| 53 Portand, OR |  |  |
| 54 Roleigh, NC |  |  |
| 55 Richmond, VA |  |  |
| 56 Sacromento, CA |  |  |
| 57 Salt Lake City, UT |  |  |
| 58 Son Antonio. TX |  |  |
| 59 Son Diego, CA |  |  |
| 60 Son Froncisco, CA |  |  |
| 61 Seottle,Tocomo,WA |  |  |
| 62 Soult St. Marie, M1 |  |  |
| 63 Saint Louls. MO |  |  |
| 64 Tampo, fL |  |  |
| 65 Tulsa, OX |  |  |
| 66 Woshington, DC |  |  |



Figure 2 Monthly autocorrelations.

Figure 2 presents a summary of the monthly results. There is a rather consistent trend. The average autocorrelation coefficient is largest in the cold months and lowest in the hot months. The same trend is exhibited by the standard deviations.

## Comparisons of Predicted CDH74 Against the 101 Hourly Weather Tapes

Figure 3 presents a comparison of the annual CDH74 calculated using the average autocorrelation coefficients and the annual CDH74 extracted from the 101 hourly tapes. The statistical correlation coefficient for the data is 0.904 . The scatter is attributed to using an average autocorrelation coefficient, defining the average in $10^{\circ} \mathrm{F}$ intervals, and ignoring any location dependence such as coastal effects or elevation differences.

## Extrapolations

The average autocorrelation coefficients derived from the 101 hourly tapes did not cover all climatic conditions that exist in the United States and Canada. To apply the calculation procedure to the 3,349 locations in the United States and the 1,847 locations in Canada the average autocorrelation coefficient had to be extrapolated to account for the extreme climatic conditions.

The data base of monthly average dry-bulb temperatures for 3,349 locations in the United States and the

TABLE 2 Average Autocorrelation Coefficients by Month and $10^{\circ} \mathrm{F}$ Intervals

| Temperature Intervals in $10^{\circ} \mathrm{F}$ Increments |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | MIN MAX | -40 -30 | $\begin{aligned} & -30 \\ & -20 \end{aligned}$ | $\begin{aligned} & -20 \\ & -10 \end{aligned}$ | $\begin{array}{r} -10 \\ 0 \end{array}$ | $\begin{array}{r} 0 \\ 10 \end{array}$ | $\begin{aligned} & 10 \\ & 20 \end{aligned}$ | $\begin{aligned} & 20 \\ & 30 \end{aligned}$ | $\begin{aligned} & 30 \\ & 40 \end{aligned}$ | $\begin{aligned} & 40 \\ & 50 \end{aligned}$ | $\begin{aligned} & 50 \\ & 60 \end{aligned}$ | $\begin{aligned} & 60 \\ & 70 \end{aligned}$ | $\begin{aligned} & 70 \\ & 80 \end{aligned}$ | $\begin{aligned} & 80 \\ & 90 \end{aligned}$ | $\begin{array}{r} 90 \\ 100 \end{array}$ | $\begin{aligned} & 100 \\ & 110 \end{aligned}$ | $\begin{aligned} & \text { MON } \\ & \text { AVG } \end{aligned}$ |
| JAN | $\begin{aligned} & \text { No. } \\ & r_{\text {jvg }} \\ & r_{\text {SD }} \end{aligned}$ | $\begin{gathered} 0 \\ .049 \\ \hline \end{gathered}$ | $\begin{array}{r} 0 \\ .069 \\ \hline \end{array}$ | $\begin{gathered} 0 \\ .087 \\ \hline \end{gathered}$ | $\begin{gathered} 0 \\ .105 \\ \hline \end{gathered}$ | $\begin{aligned} & 4 \\ & .124 \\ & .025 \end{aligned}$ | $\begin{gathered} 5 \\ .143 \\ .026 \end{gathered}$ | $\begin{gathered} 22 \\ .153 \\ .052 \end{gathered}$ | $\begin{gathered} 21 \\ .182 \\ .109 \end{gathered}$ | $\begin{aligned} & 28 \\ & .147 \\ & .078 \end{aligned}$ | $\begin{aligned} & 13 \\ & .125 \\ & .045 \end{aligned}$ | $\begin{aligned} & 4 \\ & .180 \\ & .032 \end{aligned}$ | $\begin{gathered} 0 \\ .180 \\ \hline \end{gathered}$ | $\begin{gathered} 0 \\ .180 \\ \hline \end{gathered}$ | 0 | 0 | $\begin{gathered} 97 \\ .153 \\ .074 \end{gathered}$ |
| FEB | $\begin{aligned} & \text { NO. } \\ & r_{\mathrm{JVg}} \\ & \mathrm{r}_{S D} \end{aligned}$ | $\begin{gathered} 0 \\ .029 \\ \hline \end{gathered}$ | $\begin{gathered} 0 \\ .060 \\ \hline \end{gathered}$ | $\begin{gathered} 0 \\ .092 \\ \hline \end{gathered}$ | $\begin{gathered} 0 \\ .123 \\ \hline \end{gathered}$ | $\begin{aligned} & 1 \\ & .160 \\ & N A \end{aligned}$ | $\begin{gathered} 6 \\ .172 \\ .029 \end{gathered}$ | $\begin{gathered} 14 \\ .237 \\ .146 \end{gathered}$ | $\begin{gathered} 21 \\ .244 \\ .131 \end{gathered}$ | $\begin{gathered} 31 \\ .164 \\ .089 \end{gathered}$ | $\begin{gathered} 19 \\ .169 \\ .079 \end{gathered}$ | $\begin{gathered} 5 \\ .176 \\ .064 \end{gathered}$ | $\begin{gathered} 0 \\ .182 \\ \hline \end{gathered}$ | $\begin{gathered} 0 \\ .188 \\ \hline \end{gathered}$ | 0 | 0 | $\begin{gathered} 97 \\ .194 \\ .108 \end{gathered}$ |
| MAR | $\begin{aligned} & \text { NO. } \\ & r_{\mathrm{dvg}} \\ & \mathrm{r}_{\mathrm{sO}} \end{aligned}$ | $\begin{array}{r} 0 \\ +251 \\ \hline \end{array}$ | $\begin{gathered} 0 \\ .236 \\ \hline \end{gathered}$ | $\begin{gathered} 0 \\ 221 \\ \hline \end{gathered}$ | $\begin{gathered} 0 \\ 206 \\ \hline \end{gathered}$ | $\begin{gathered} 0 \\ .191 \\ \hline \end{gathered}$ | $\begin{gathered} 1 \\ -177 \\ \hline \text { NA } \end{gathered}$ | $\begin{gathered} 4 \\ \frac{.162}{N A} \end{gathered}$ | $\begin{aligned} & 20 \\ & .157 \\ & .102 \end{aligned}$ | $\begin{gathered} 27 \\ .113 \\ .043 \end{gathered}$ | $\begin{gathered} 34 \\ .127 \\ .063 \end{gathered}$ | $\begin{gathered} 9 \\ .103 \\ .043 \end{gathered}$ | $\begin{aligned} & 2 \\ & .185 \\ & .003 \end{aligned}$ | $\begin{gathered} 0 \\ .185 \\ \hline \end{gathered}$ | 0 | 0 | $\begin{gathered} 97 \\ .139 \\ .088 \end{gathered}$ |
| APR | $\begin{aligned} & \text { NO. } \\ & r_{\text {dvg }} \\ & r_{\text {SD }} \end{aligned}$ | 0 | 0 | $\begin{gathered} 0 \\ .149 \\ \hline \end{gathered}$ | $\begin{gathered} 0 \\ .140 \\ \hline \end{gathered}$ | $\begin{gathered} 0 \\ .131 \\ \hline \end{gathered}$ | $\begin{gathered} 0 \\ .122 \\ \hline \end{gathered}$ | $\begin{gathered} 0 \\ .113 \\ \hline \end{gathered}$ | $\begin{aligned} & 5 \\ & .125 \\ & .060 \end{aligned}$ | $\begin{gathered} 18 \\ .073 \\ .021 \end{gathered}$ | $\begin{gathered} 42 \\ .077 \\ .038 \end{gathered}$ | $\begin{gathered} 25 \\ .073 \\ .025 \end{gathered}$ | $\begin{aligned} & 7 \\ & .080 \\ & .030 \end{aligned}$ | $\begin{gathered} 0 \\ .075 \\ \hline \end{gathered}$ | 0 | 0 | $\begin{gathered} 97 \\ .078 \\ .034 \end{gathered}$ |
| MAY | $\begin{aligned} & \text { NO. } \\ & r_{\text {avg }} \\ & r_{\text {SO }} \end{aligned}$ | 0 | 0 | 0 | 0 | 0 | $\begin{gathered} 0 \\ -081 \\ \hline \end{gathered}$ | $\begin{gathered} 0 \\ 0.081 \\ \hline \end{gathered}$ | $\begin{gathered} 0 \\ -081 \\ \hline \end{gathered}$ | $\begin{gathered} 2 \\ .062 \\ .003 \end{gathered}$ | $\begin{gathered} 26 \\ .087 \\ .035 \end{gathered}$ | $\begin{gathered} 41 \\ .085 \\ .035 \end{gathered}$ | $\begin{gathered} 26 \\ .070 \\ .031 \end{gathered}$ | $\begin{gathered} 2 \\ .083 \\ .057 \end{gathered}$ | 0 | 0 | $\begin{gathered} 97 \\ .081 \\ .034 \end{gathered}$ |
| JUN | $\begin{aligned} & \text { NO. } \\ & r_{\text {ovg }} \\ & r_{\text {so }} \end{aligned}$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\begin{gathered} 0 \\ .076 \\ \hline \end{gathered}$ | $\begin{gathered} 0 \\ .076 \\ \hline \end{gathered}$ | $\begin{aligned} & 7 \\ & .086 \\ & .022 \end{aligned}$ | $\begin{gathered} 35 \\ .078 \\ .056 \end{gathered}$ | $\begin{gathered} 42 \\ .077 \\ .035 \end{gathered}$ | $\begin{gathered} 13 \\ .064 \\ .015 \end{gathered}$ | $\begin{gathered} 0 \\ .064 \\ \hline \end{gathered}$ | 0 | $\begin{gathered} 97 \\ .076 \\ .041 \end{gathered}$ |
| JUL | NO. <br> $r_{\text {dvg }}$ <br> $\Gamma_{\text {SO }}$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\begin{gathered} 0 \\ .068 \\ \hline \end{gathered}$ | $\begin{gathered} 0 \\ .068 \\ \hline \end{gathered}$ | $\begin{aligned} & 1 \\ & .042 \\ & \mathrm{NA} \end{aligned}$ | $\begin{gathered} 19 \\ .080 \\ .058 \end{gathered}$ | $\begin{gathered} 52 \\ .062 \\ .034 \end{gathered}$ | $\begin{gathered} 21 \\ .080 \\ .047 \end{gathered}$ | $\begin{gathered} 4 \\ .033 \\ .011 \end{gathered}$ | $\begin{gathered} 0 \\ .033 \\ \hline \end{gathered}$ | $\begin{gathered} 97 \\ .068 \\ .043 \end{gathered}$ |
| AUG | NO. <br> $r_{\text {dvg }}$ <br> $r_{50}$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\begin{gathered} 0 \\ .072 \\ \hline \end{gathered}$ | $\begin{gathered} 0 \\ .072 \\ \hline \end{gathered}$ | $\begin{gathered} 2 \\ .054 \\ .026 \end{gathered}$ | $\begin{gathered} 20 \\ .116 \\ .090 \end{gathered}$ | $\begin{gathered} 55 \\ .061 \\ .028 \end{gathered}$ | $\begin{aligned} & 19 \\ & .069 \\ & .025 \end{aligned}$ | $\begin{aligned} & 1 \\ & .040 \\ & \text { NA } \end{aligned}$ | 0 | $\begin{gathered} 97 \\ .072 \\ .052 \end{gathered}$ |
| SEP | NO. <br> $r_{\text {avg }}$ <br> $\Gamma_{S O}$ | 0 | 0 | 0 | 0 | 0 | $\begin{gathered} 0 \\ .079 \\ \hline \end{gathered}$ | $\begin{gathered} 0 \\ .079 \\ \hline \end{gathered}$ | $\begin{gathered} 0 \\ .079 \\ \hline \end{gathered}$ | $\begin{gathered} 0 \\ .079 \\ \hline \end{gathered}$ | $\begin{gathered} 14 \\ .063 \\ .028 \end{gathered}$ | $\begin{aligned} & .40 \\ & .086 \\ & .057 \end{aligned}$ | $\begin{aligned} & 35 \\ & .082 \\ & .043 \end{aligned}$ | $\begin{gathered} 8 \\ .066 \\ .038 \end{gathered}$ | $\begin{gathered} 0 \\ .079 \\ \hline \end{gathered}$ | 0 | $\begin{gathered} 97 \\ .079 \\ .048 \end{gathered}$ |
| OCT | $\begin{aligned} & \text { NO. } \\ & \mathbf{r}_{\text {dug }} \\ & \mathrm{r}_{\mathrm{SD}} \end{aligned}$ | 0 | 0 | 0 | $\begin{gathered} 0 \\ .079 \\ \hline \end{gathered}$ | $\begin{gathered} 0 \\ .079 \\ \hline \end{gathered}$ | $\begin{gathered} 0 \\ .079 \\ \hline \end{gathered}$ | $\begin{gathered} 0 \\ -079 \\ \hline \end{gathered}$ | $\begin{gathered} 0 \\ .079 \\ \hline \end{gathered}$ | $\begin{gathered} 14 \\ .084 \\ .035 \end{gathered}$ | $\begin{aligned} & 38 \\ & .080 \\ & .033 \end{aligned}$ | $\begin{gathered} 37 \\ .078 \\ .034 \end{gathered}$ | $\begin{aligned} & 8 \\ & .071 \\ & .034 \end{aligned}$ | $\begin{gathered} 0 \\ .079 \\ \hline \end{gathered}$ | 0 | 0 | $\begin{gathered} 97 \\ .079 \\ .033 \end{gathered}$ |
| NOV | $\begin{aligned} & \text { NO. } \\ & r_{\mathrm{dvg}} \\ & \mathrm{r}_{\mathrm{SO}} \end{aligned}$ | $\begin{gathered} 0 \\ .199 \\ \hline \end{gathered}$ | $\begin{gathered} 0 \\ .199 \\ \hline \end{gathered}$ | $\begin{gathered} 0 \\ -199 \\ \hline \end{gathered}$ | $\begin{gathered} 0 \\ .199 \\ \hline \end{gathered}$ | $\begin{gathered} 0 \\ -199 \\ \hline \end{gathered}$ | $\begin{gathered} 0 \\ .199 \\ \hline \end{gathered}$ | $\begin{aligned} & 3 \\ & .199 \\ & .058 \end{aligned}$ | $\begin{gathered} 13 \\ .136 \\ .074 \end{gathered}$ | $\begin{gathered} .36 \\ .090 \\ .036 \end{gathered}$ | $\begin{aligned} & 33 \\ & .077 \\ & .035 \end{aligned}$ | $\begin{gathered} 10 \\ .104 \\ .024 \end{gathered}$ | $\begin{aligned} & 2 \\ & .155 \\ & .131 \end{aligned}$ | $\begin{gathered} 0 \\ .190 \\ \hline \end{gathered}$ | 0 | 0 | $\begin{gathered} 97 \\ .098 \\ .051 \end{gathered}$ |
| DEC | $\begin{aligned} & \text { No. } \\ & r_{\mathrm{dvg}} \\ & \mathrm{r}_{\mathrm{SO}} \end{aligned}$ | $\begin{gathered} 0 \\ .192 \\ \hline \end{gathered}$ | $\begin{gathered} 0 \\ .192 \\ \hline \end{gathered}$ | $\begin{gathered} 0 \\ .192 \\ \hline \end{gathered}$ | $\begin{gathered} 0 \\ .192 \\ \hline \end{gathered}$ | $\begin{gathered} 0 \\ .192 \\ \hline \end{gathered}$ | $\begin{aligned} & 5 \\ & .197 \\ & .095 \end{aligned}$ | $\begin{gathered} 13 \\ .192 \\ .116 \end{gathered}$ | $\begin{gathered} 26 \\ .187 \\ .112 \end{gathered}$ | $\begin{gathered} 31 \\ .120 \\ .054 \end{gathered}$ | $\begin{gathered} 17 \\ .104 \\ .047 \end{gathered}$ | $\begin{gathered} 4 \\ .106 \\ .017 \end{gathered}$ | $\begin{aligned} & 1 \\ & .249 \\ & \mathrm{NA} \end{aligned}$ | 0 $.149$ | 0 | 0 | $\begin{gathered} 97 \\ .149 \\ .090 \end{gathered}$ |

Notes: Average autocorrelations underlined were extrapolated using Figures 2-13. NA = Not Avallable

## CDH74 Using Average Autocorrelation Coefficients (1000)



CDH74 From 101 Hourly Tapes (Thousands)
Flgure 3 Comparisons of CDH 74 calculated using autocorrelations vs, hourly weather data tapes.

1,847 locations in Canada was analyzed to determine whether the 1,212 months of hourly results accounted for the entire range of monthly temperatures. Table 3 presents the number of months within the $10^{\circ} \mathrm{F}$ tempera-
ture intervals contained in the United States temperature data base and Table 4 presents the number of months contained in the Canadian temperature data base. The underlined values represent the months where data exist in the respective country but not in the 101 hourly tapes.

The United States data base contained 40,188 months, and only 527 months, or $1.3 \%$, were not covered by the 1,212 months available on hourly weather tapes. The majority of the extrapolations were in temperature intervals at or below $45^{\circ} \mathrm{F}$ and have no major impact in determining CDH74. The extrapolations in the temperature intervals of $75^{\circ} \mathrm{F}$ and above would have an impact in calculating CDH74. These extrapolations accounted for 112 months, which was only $0.27 \%$ of the total.

The Canadian data base contained 22,164 months, and 3,496 months, or $15.8 \%$, were not covered by the 1,212 months available on hourly weather tapes. All of the extrapolations were in temperature intervals at or below $45^{\circ} \mathrm{F}$ and have no major impact in determining CDH74.

The basis for the extrapolations varied, depending on the specific data for each month. Furthermore, it also varied above and below the monthly average temperature. For example, in January, extrapolations below the monthly average temperature were based on extending the trend between $35^{\circ} \mathrm{F}$ and $5^{\circ} \mathrm{F}$ down to $-35^{\circ} \mathrm{F}$. Above the monthly average temperature, the extrapolation consisted of just repeating the average value at $65^{\circ} \mathrm{F}$ for $75^{\circ} \mathrm{F}$ and $85^{\circ} \mathrm{F}$.

TABLE 3 Number of Months in $10^{\circ} \mathrm{F}$ Intervals for the Unifed States

| Temperature intervals in $10^{\circ} \mathrm{F}$ Increments |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MIN | -30 | -20 | -10 | 0 | 10 | 20 | 30 | 40 | 50 | 60 | 70 | 80 | 90 | 100 |
| MAX | -20 | -10 | 0 | 10 | 20 | 30 | 40 | 50 | 60 | 70 | 80 | 90 | 100 | 110 |
| JAN | 1 | 7 | 14 | 188 | 541 | 1011 | 770 | 541 | 197 | 47 | 25 | 7 | 0 | 0 |
| FEB | $\underline{1}$ | 1 | 9 | 38 | 387 | 881 | 947 | 664 | 327 | 62 | 25 | 7 | 0 | 0 |
| MAR | 0 | $\underline{2}$ | $\underline{1}$ | 7 | 21 | 468 | 1110 | 915 | 615 | 168 | 35 | 7 | 0 | 0 |
| APR | 0 | 0 | $\underline{2}$ | 0 | $\underline{2}$ | 11 | 196 | 1359 | 1031 | 625 | 116 | 7 | 0 | 0 |
| MAY | 0 | 0 | 0 | 0 | 1 | 1 | 8 | 160 | 1419 | 1218 | 530 | 12 | 0 | 0 |
| Jun | 0 | 0 | 0 | 0 | 0 | 0 | $\underline{2}$ | 17 | 336 | 1450 | 1314 | 229 | 1 | 0 |
| JuL | 0 | 0 | 0 | 0 | 0 | 0 | $\underline{2}$ | 4 | 85 | 798 | 1771 | 655 | 33 | 1 |
| AUG | 0 | 0 | 0 | 0 | 0 | 0 | $\underline{2}$ | $\underline{4}$ | 109 | 1101 | 1595 | 521 | 17 | 0 |
| SEP | 0 | 0 | 0 | 0 | 0 | 0 | $\underline{2}$ | 56 | 811 | 1492 | 859 | 128 | 1 | 0 |
| OCT | 0 | 0 | 0 | 0 | $\underline{3}$ | 13 | 31 | 877 | 1496 | 750 | 165 | 14 | 0 | 0 |
| NOV | 0 | 0 | $\underline{4}$ | 10 | $\underline{4}$ | 226 | 1152 | 1127 | 635 | 138 | 43 | $\underline{10}$ | 0 | 0 |
| DEC | 0 | 7 | 7 | 19 | 332 | 969 | 998 | 682 | 246 | 53 | 29 | 7 | 0 | 0 |
| TOT | 2 | 17 | 37 | 262 | 1291 | 3580 | 5220 | 6406 | 7307 | 7902 | 6507 | 1604 | 52 | 1 |

Note: Underlined values represent months which exceeded temperature ranges of 101 hourly tapes.

Temperature Intervals in $10^{\circ} \mathrm{F}$ Increments

| MIN | -50 | -40 | -30 | -20 | -10 | 0 | 10 | 20 | 30 | 40 | 50 | 60 | 70 | 80 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MAX | -40 | -30 | -20 | -10 | 0 | 10 | 20 | 30 | 40 | 50 | 60 | 70 | 80 | 90 |
| JAN | 0 | 4 | 40 | 60 | 371 | 417 | 517 | 297 | 138 | 3 | 0 | 0 | 0 | 0 |
| FEB | 0 | 7 | 28 | $\underline{28}$ | 75 | 488 | 663 | 367 | 128 | 63 | 0 | 0 | 0 | 0 |
| MAR | 0 | $\underline{2}$ | 14 | $\underline{25}$ | $\underline{21}$ | 47 | 481 | 864 | 272 | 121 | 0 | 0 | 0 | 0 |
| APR | 0 | 0 | 0 | 5 | 23 | 18 | $\underline{23}$ | 64 | 1128 | 583 | 3 | 0 | 0 | 0 |
| MAY | 0 | 0 | 0 | 0 | 0 | 0 | $\underline{27}$ | $\underline{22}$ | 47 | 763 | 988 | 0 | 0 | 0 |
| Jun | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 44 | 69 | 1033 | 701 | 0 | 0 |
| JUL | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 11 | 36 | 287 | 1452 | 61 | 0 |
| AUG | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 15 | 37 | 508 | 1263 | 24 | 0 |
| SEP | 0 | 0 | 0 | 0 | 0 | 0 | $\underline{3}$ | 15 | $\underline{35}$ | 344 | 1341 | 109 | 0 | 0 |
| OCT | 0 | 0 | 0 | 0 | $\underline{3}$ | $\underline{5}$ | 34 | 40 | 316 | 1330 | 119 | 0 | 0 | 0 |
| Nov | 0 | 0 | 1 | 11 | 30 | 36 | 129 | 709 | 743 | 188 | 0 | 0 | 0 | 0 |
| DEC | 0 | 1 | 11 | $\underline{47}$ | 58 | 451 | 591 | 492 | 170 | 26 | 0 | 0 | 0 | 0 |
| TOT | 0 | 14 | 94 | 176 | 1581 | 1462 | 2468 | 2870 | 3047 | 3563 | 4279 | 3525 | 85 | 0 |

Note: Underlined volues represent months which exceeded temperature ranges of 101 hourly tapes.

## CDH74 Calculation Procedure

The calculation procedure starts by determining the standard deviation of the dry-bulb temperature within a month. This requires using the data base of monthly average dry-bulb temperatures and the monthly standard deviations plus the average autocorrelation coefficients from Table 2 in Equation 2:

$$
\begin{equation*}
\sigma_{T_{t}}=\frac{\sqrt{N H_{i}} \cdot \sigma_{N, i}}{\sqrt{1+\left(N H_{i}-1\right) \cdot r_{A V G_{i, j}}}} \tag{2}
\end{equation*}
$$

where

$$
\begin{aligned}
& r_{A V G_{i j}}= \text { average autocorrelation coeffi- } \\
& \text { cient for the } i^{\text {th }} \text { month and the } \\
& j^{\text {th }} \text { temperature interval (dimen- } \\
& \text { sionless). }
\end{aligned}
$$

Then CDH74 was calculated by integrating a normal distribution curve from a lower limit of $74^{\circ} \mathrm{F}$ to an upper limit defined as three standard deviations above the monthly average dry-bulb temperature. The integration was performed using standard mathematical functions (VNI 1982). All 12 months were analyzed and the results were summed to arrive at the annual CDH74.

## RESULTS

The individual city results require about 50 pages to print and are contained in ASHRAE Standard 90.2-1993.


Flgure 4 Weather data for the United States.
Considerable insight can be gained by plotting CDH74 vs. HDD65.

The U.S. results are presented in Figure 4. There are several interesting observations. First, there is a broad band between 2,000 and 10,000 HDD65, which accounts for most of the data. In general, as HDD65 increases, CDH74 decreases. It is interesting to note that the upper boundary of the broad band is so well defined. Second, there is a range of CDH74 from zero to 72,338 at HDD65 equal to zero. These primarily are from Puerto Rico, Cuba, the Virgin Islands, and the Pacific Islands. Third, the maximum CDH74 is 88,444 , which occurs at Death


Flgure 5 Weather data for Canada.

## RECOMMENDATIONS

The CDH74 calculation procedure could be improved by reducing the scatter between the calculated results and those from the hourly weather data tapes. The primary reason for the scatter was the use of statistically averaged autocorrelation coefficients for $10^{\circ} \mathrm{F}$ temperature intervals. This approach completely ignored all location dependence, such as coastal effects or elevation differences. One method to account for specific rather than average autocorrelation coefficients would be to map each city to the closest station available from the 101 hourly tapes. This would eliminate the use of statistical averages, avoid the need for extrapolation, and give some account for coastal effects and elevation. The only additional information required to perform this type of mapping would be the latitude and longitude of each city. This is readily available and should be investigated for future revisions to the standard.

Another improvement to the calculation procedure would be to use more hourly data tapes. One source would be the TMY tapes, which have 234 stations (NCDC 1981). Also, there are 116 hourly tapes available for Canada (Hsieh 1991). Using additional tapes would allow for closer mapping and should improve the overall results.

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