

Materials Challenges for Fusion Energy

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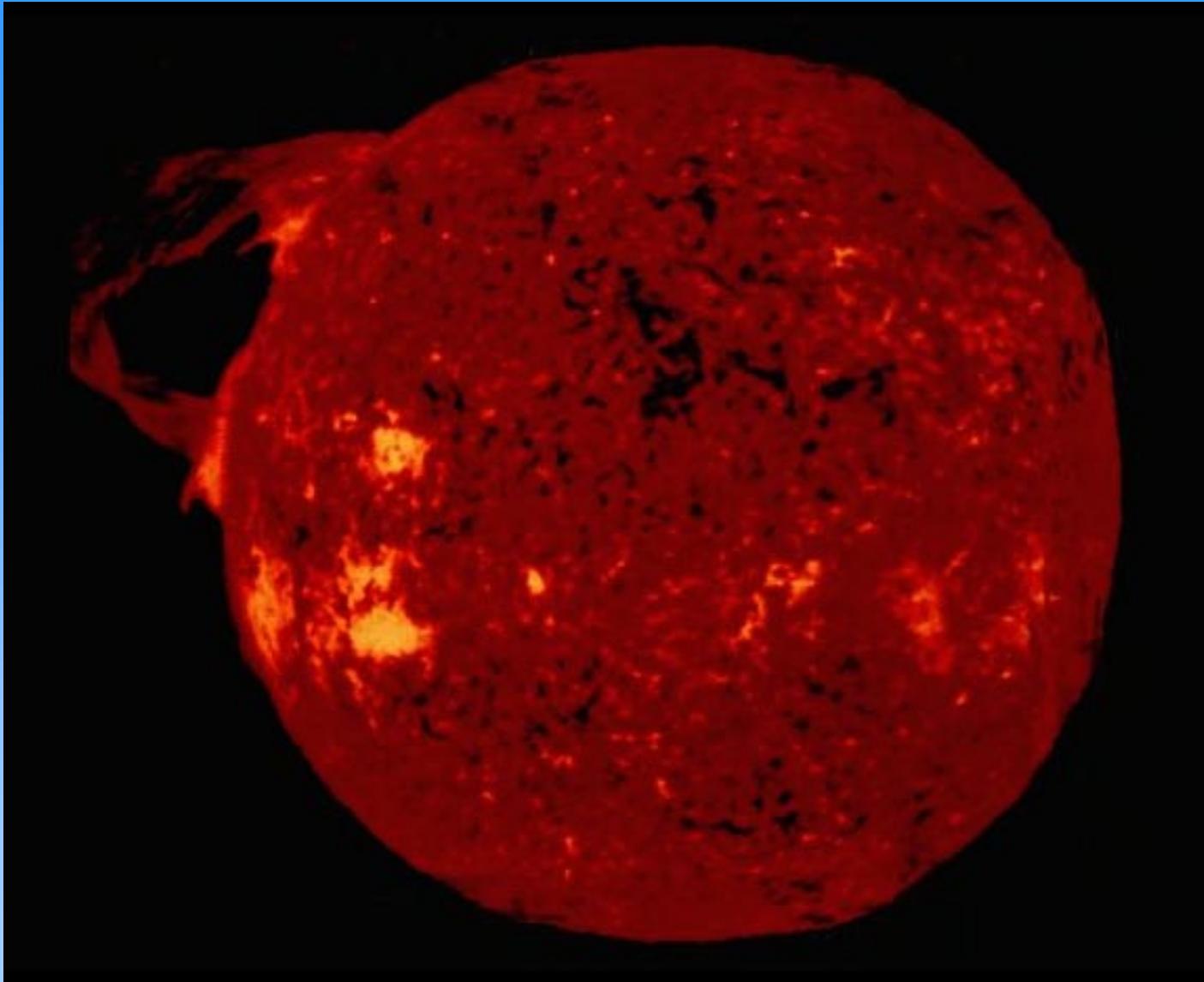
Oak Ridge National Laboratory

Oak Ridge, TN

Materials-The Opportunity

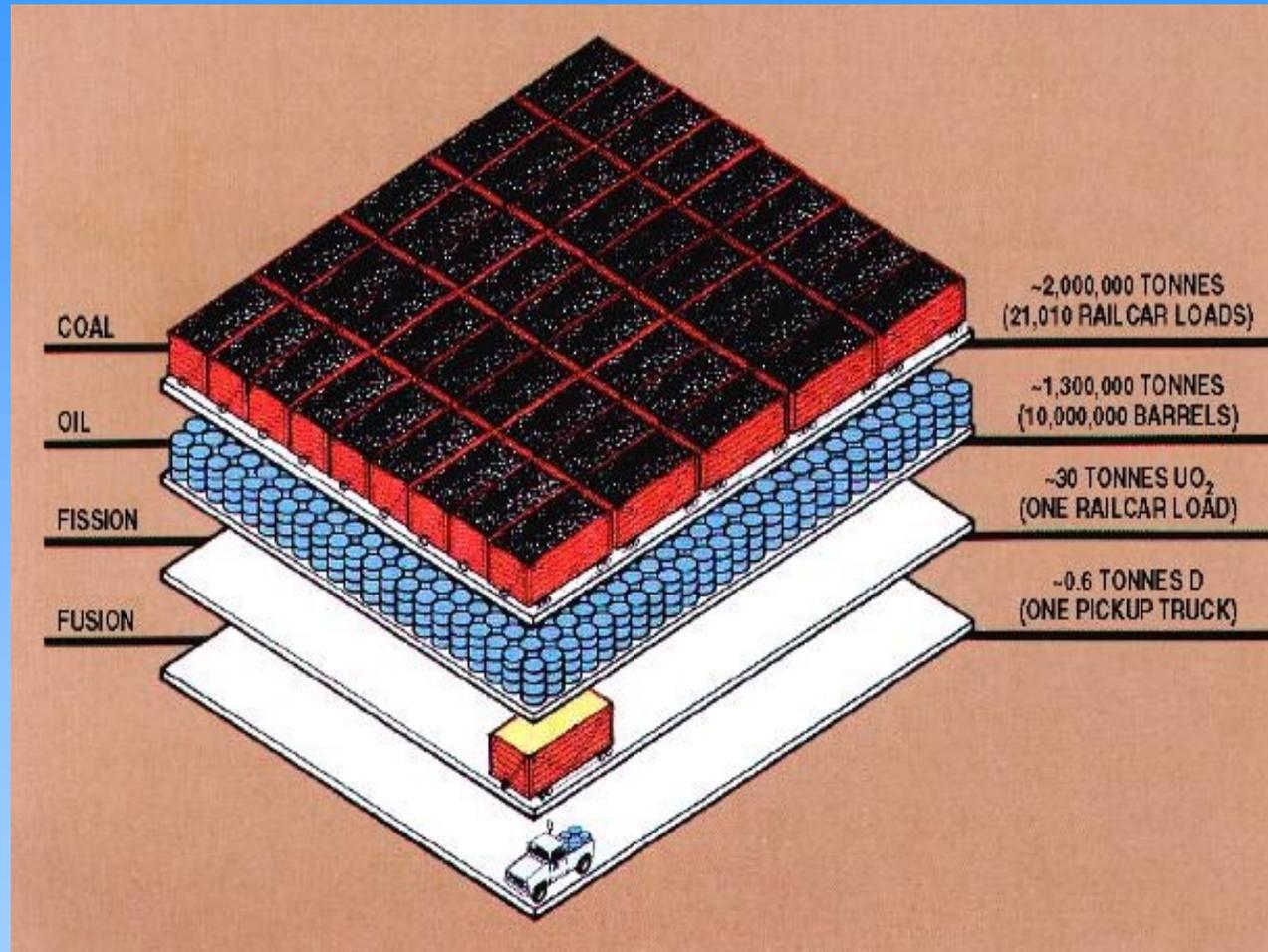
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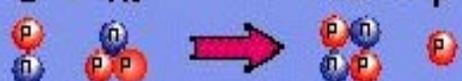
“I remain dedicated to the concept of fusion power, as a citizen, and I wish I was in a position to do more about it.” Ansel Adams, July 1983

Annual Fuel Requirements for a 700 MW_e Power Plant



One cup of water (D-D reaction) = 20 gallons of oil

Partial List of Fusion Reactions

Reaction		Ignition Temperature		Output Energy
Fuel	Product	(millions of °C)	(keV)	(keV)
$D + T$ 	${}^4\text{He} + n$	45	4	17,600
$D + {}^3\text{He}$ 	${}^4\text{He} + p$	350	30	18,300
$D + D$ 	${}^3\text{He} + n$	400	35	~4,000
	$T + p$	400	35	~4,000

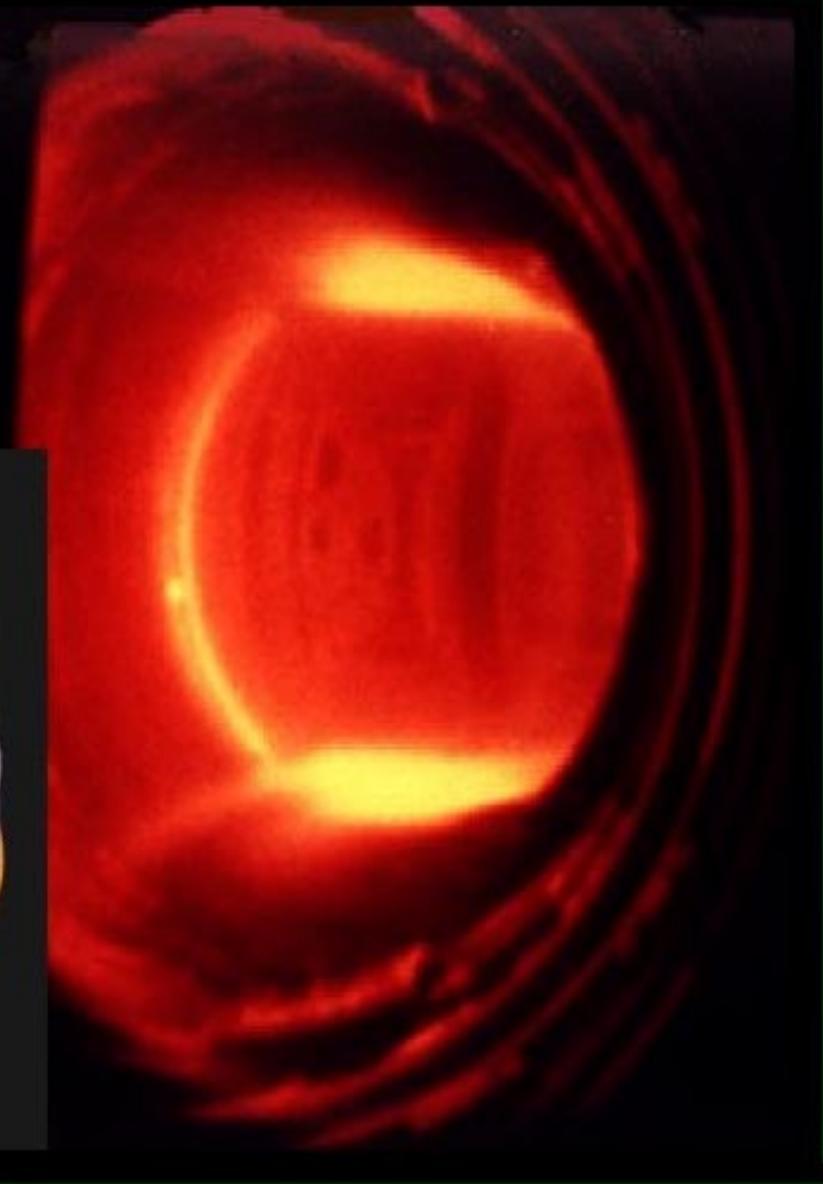
Tritium can be made from lithium ($n + \text{Li} \rightarrow \text{T} + \text{He}$)

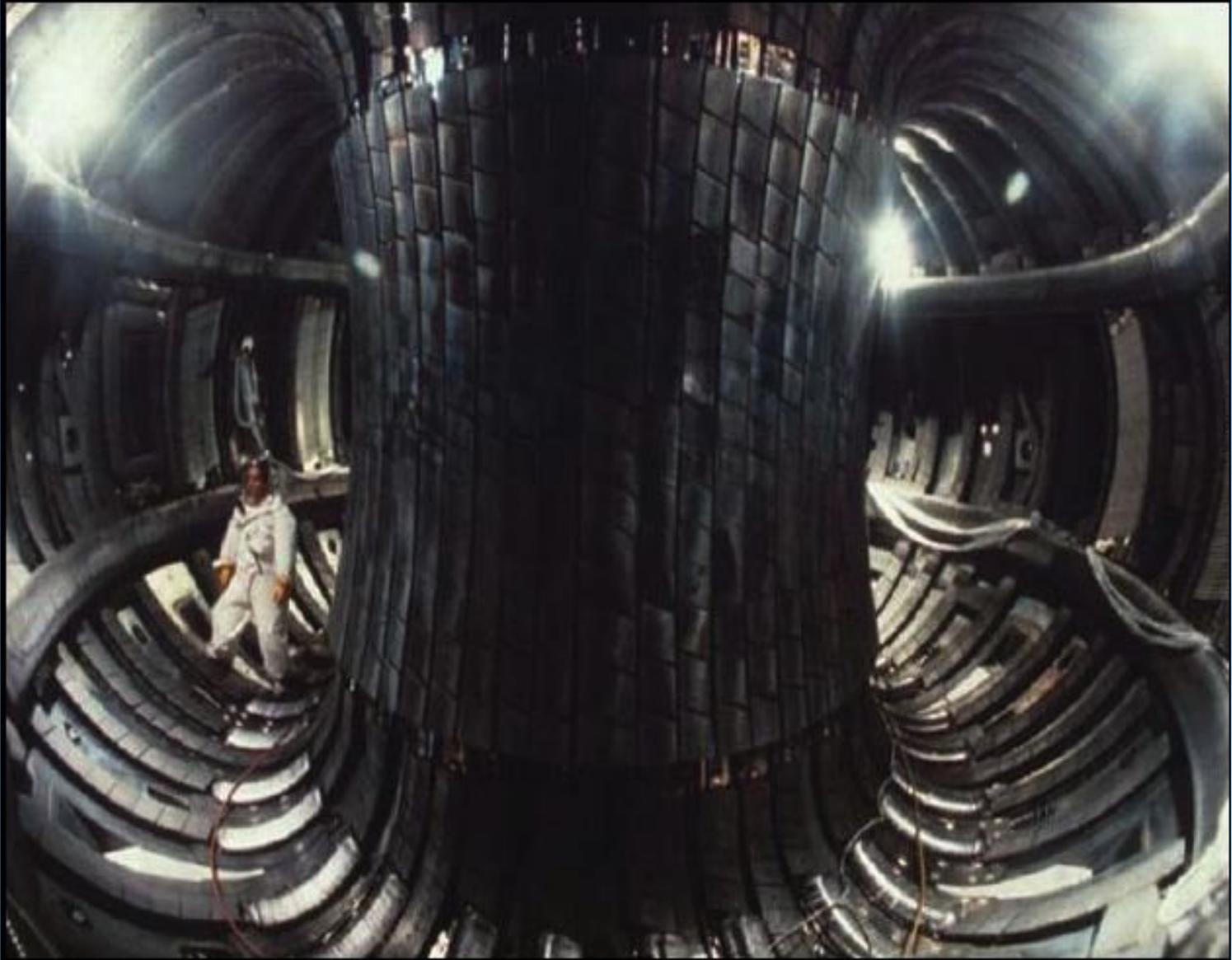
- **Neutrons produce radiation damage and bulk heating in structure**

Properties of Typical Plasmas

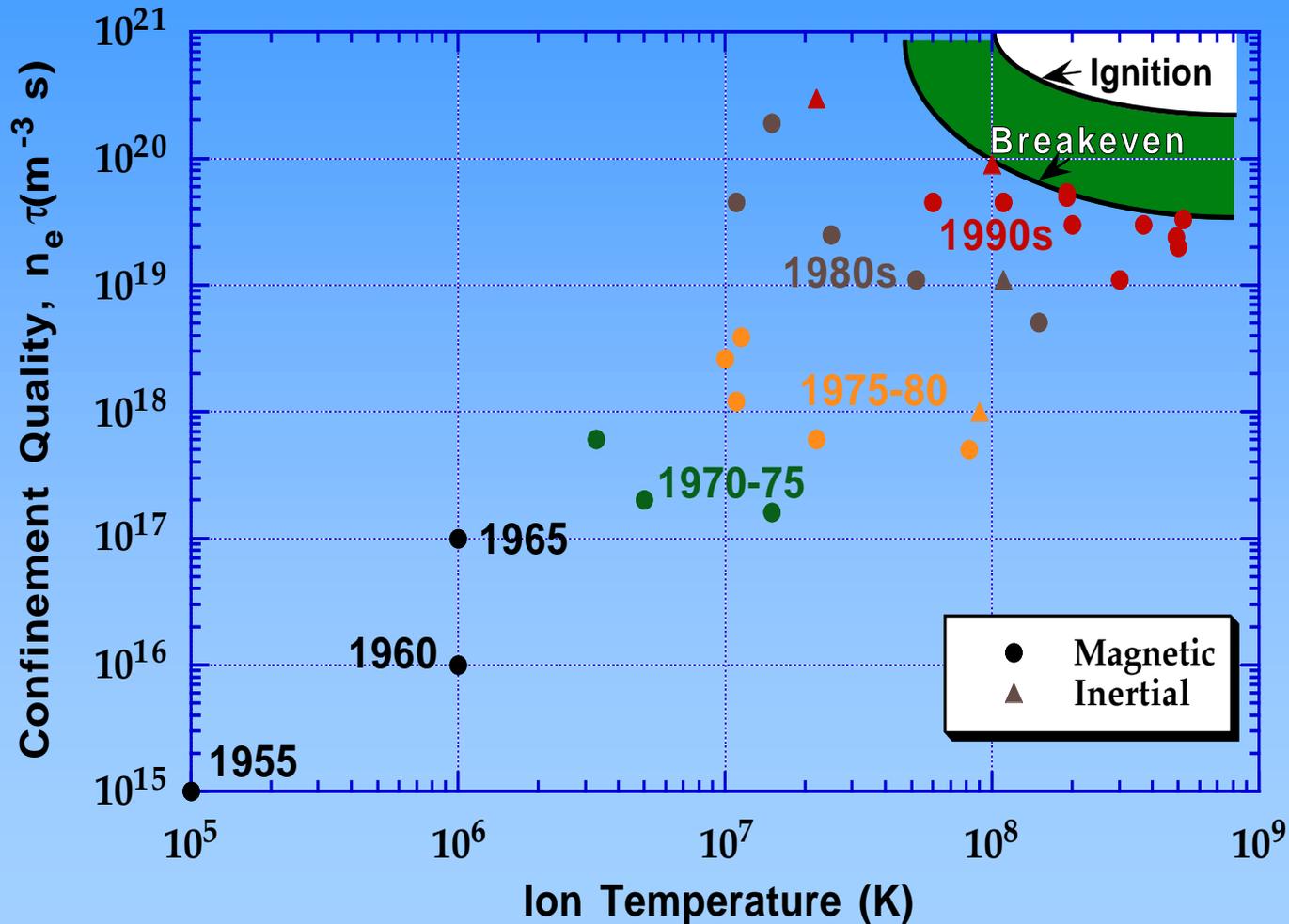
	Density	Temperature	
	$N_e \text{ (m}^{-3}\text{)}$	$T_e \text{ (eV)}$	Kelvin
Interstellar	10^6	1	10^4
Solar Corona	10^{12}	10^2	10^6
Fluorescent lamp	10^{18}	10	10^5
Magnetic fusion	10^{20}	10^4	10^8
Inertial fusion	10^{26}	10^2	10^6
Air density	10^{25}	0.025	293

Toroidal Magnetic Confinement of Plasma

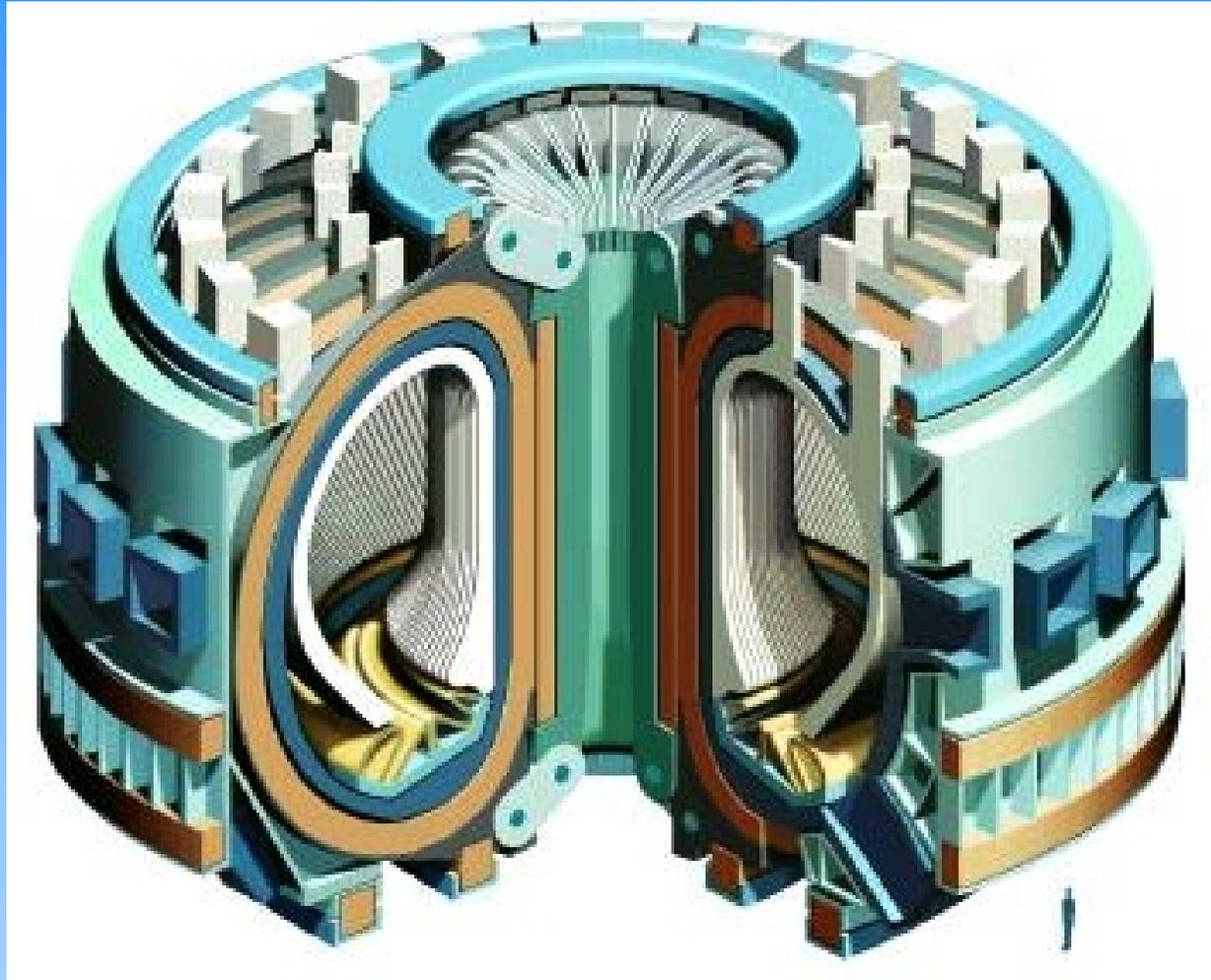




Steady Progress has led to Achievement of Breakeven Condition



ITER (International Thermonuclear Experimental Reactor)



30 meters diameter by 30 meters tall

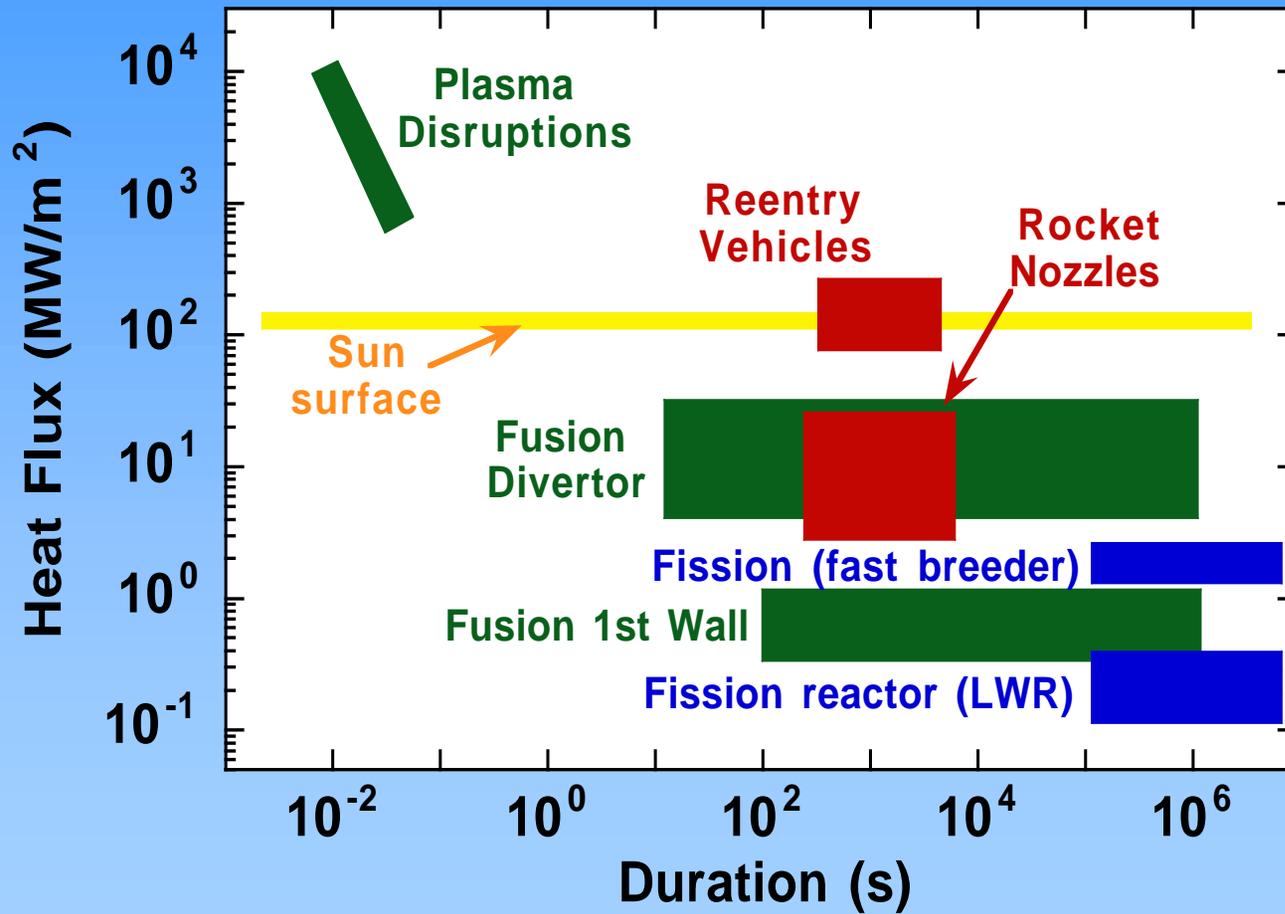
Fusion Energy R&D is at a Crossroad

- **Concept feasibility, proof of performance have been demonstrated**
- **Pathway for most attractive commercial power plant is uncertain**
 - **Magnetic vs. inertial confinement**
 - **Tokamak vs. spherical torus, stellarator, etc.**
- **Materials technology will play a major role in determining the most viable path to commercialization**

Three Examples where Materials Impact the Fusion Reactor Design

- **Plasma facing (high heat flux) components**
- **Plasma diagnostic, heating and magnet systems**
- **First wall/blanket structural materials**

Comparison of Heat Fluxes



Plasma facing (high heat flux) components

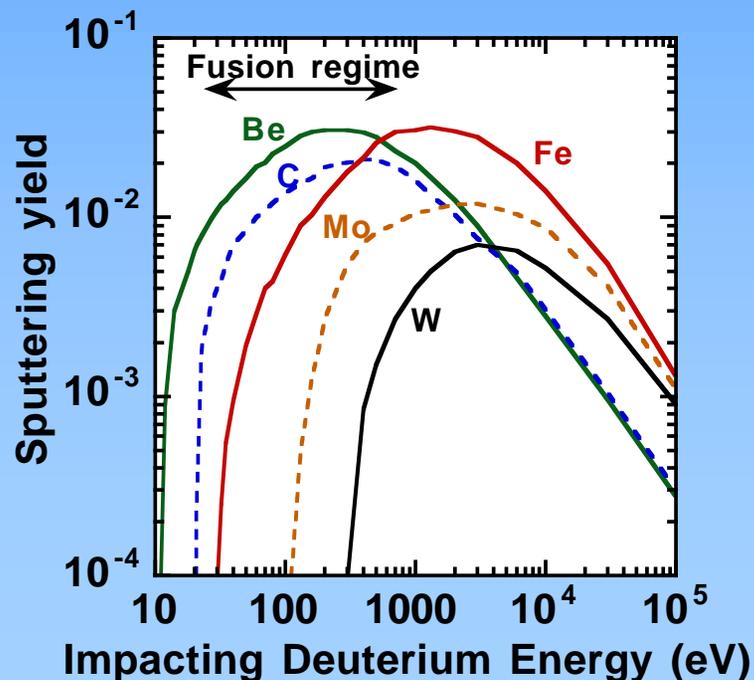
- **Capital costs can be reduced by increasing the fusion reactor power density**
- **Steady-state heat flux limit for structural materials is ~0.5 to 2 MW/m² for 5 mm walls in a fusion reactor**
 - Capacity to withstand steady state heat fluxes of >35 MW/m² has been demonstrated (He-cooled Cu divertor)
- **Carbon/carbon composites do not appear to be suitable for fusion reactors due to radiation induced thermal conductivity degradation**
- **Plasma-facing liquid coolants can provide high steady state heat flux removal capability (>2 MW/m²)**
 - Considerable technological challenges exist for application to toroidal geometry (plasma shaping, coolant vaporization, metal/coolant corrosion)

Key Factors for Plasma-Facing Materials

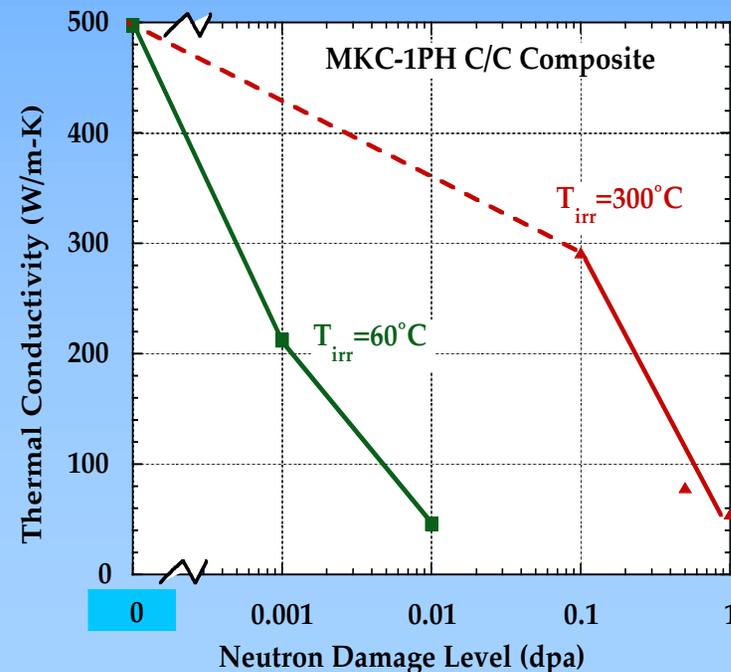
- A tradeoff exists between the amount of erosion (N) and the atomic number (Z) of the sputtered plasma-facing material

- Plasma power loss is proportional to $N_i Z_i$

- Be, C and W are the leading plasma-facing candidates



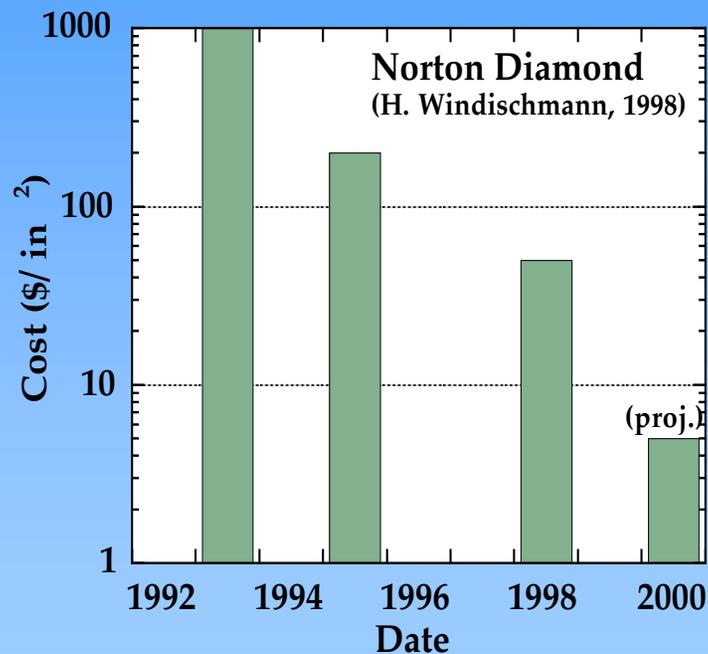
- Neutron irradiation causes a large decrease in C/C conductivity



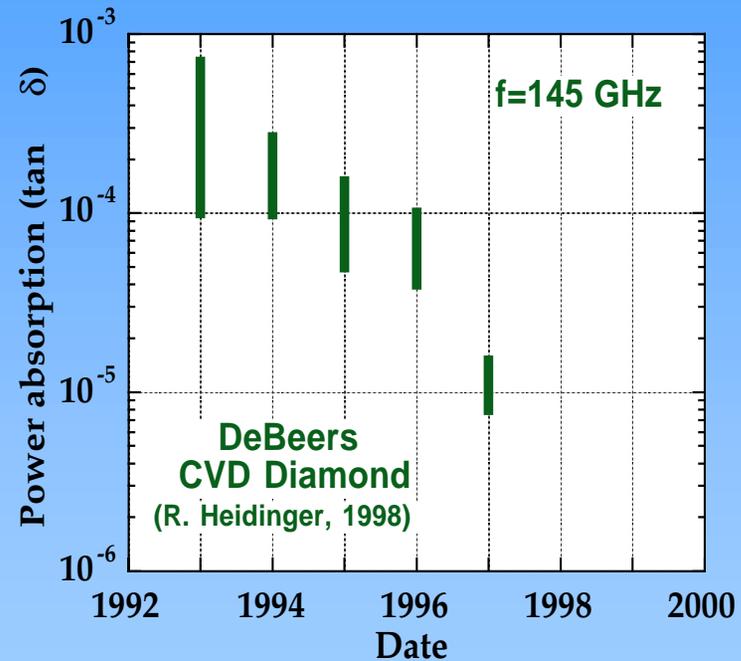
Recent Advances in CVD Diamond

Fabrication now allow High-power (~ 1 MW) Gyrotrons to be used for Plasma Heating

- CVD diamond production costs have decreased rapidly



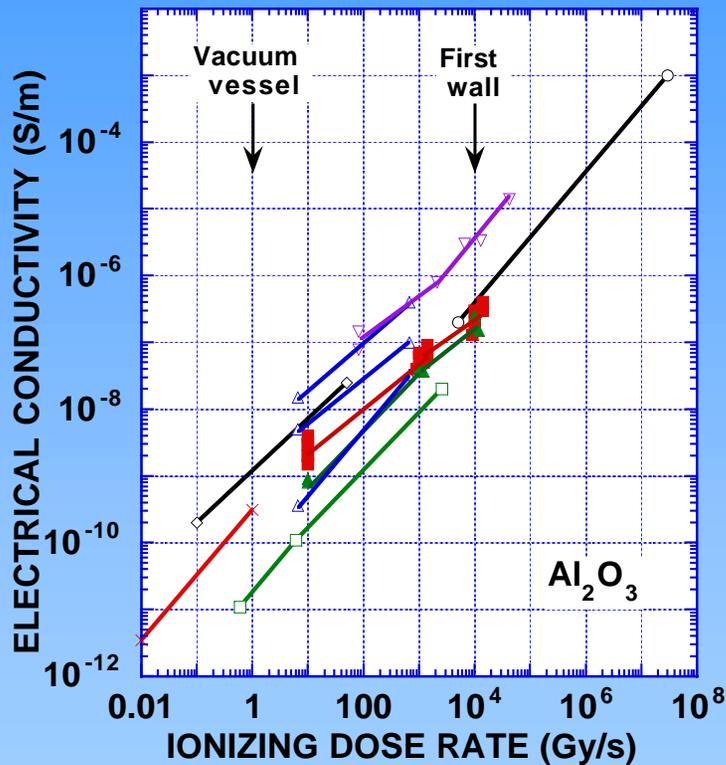
- High-quality CVD diamond (low RF power absorption) is now available



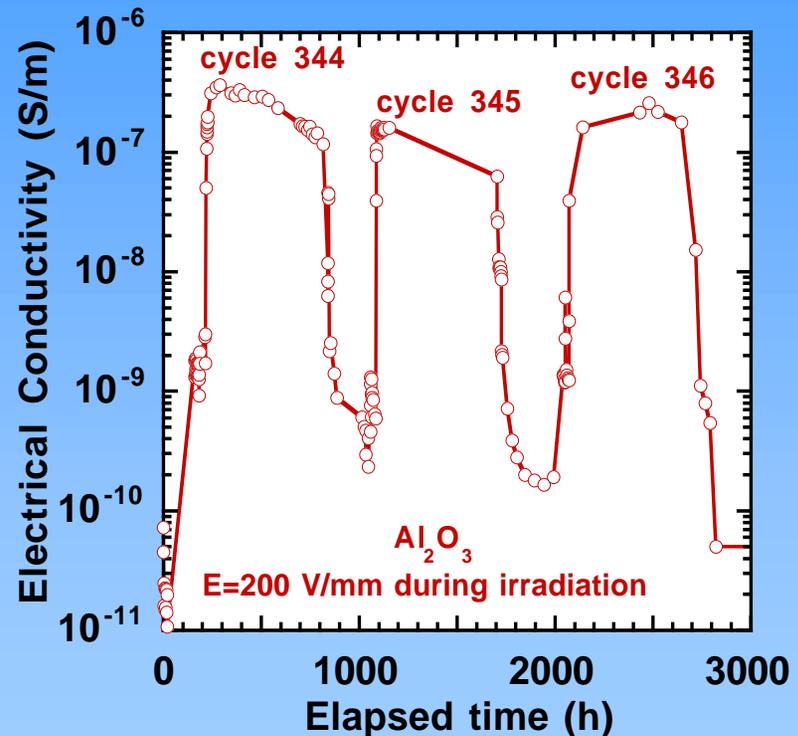
- Low power absorption is maintained in CVD diamond after irradiation to moderate neutron doses (10^3 dpa)

Ionizing Radiation Causes Large Prompt Changes in Electrical Conductivity of Insulators

- The electrical conductivity is proportional to dose rate



- No permanent degradation occurs after neutron irradiation

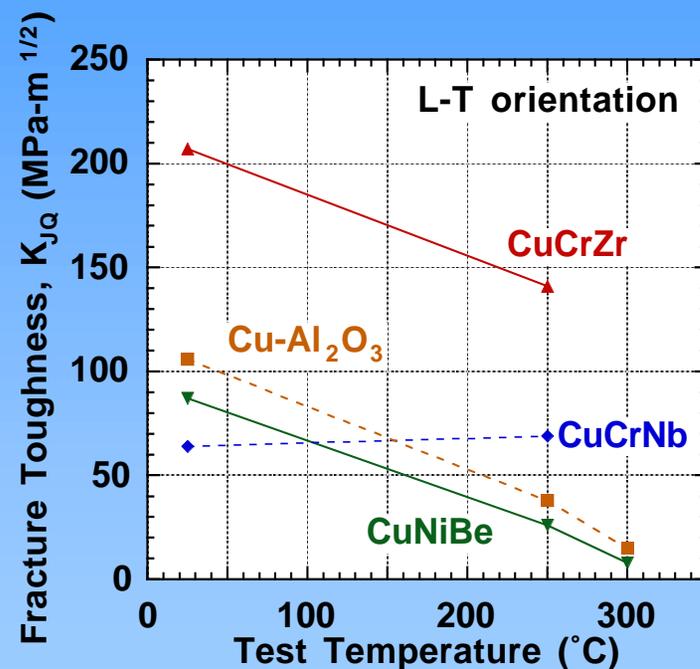
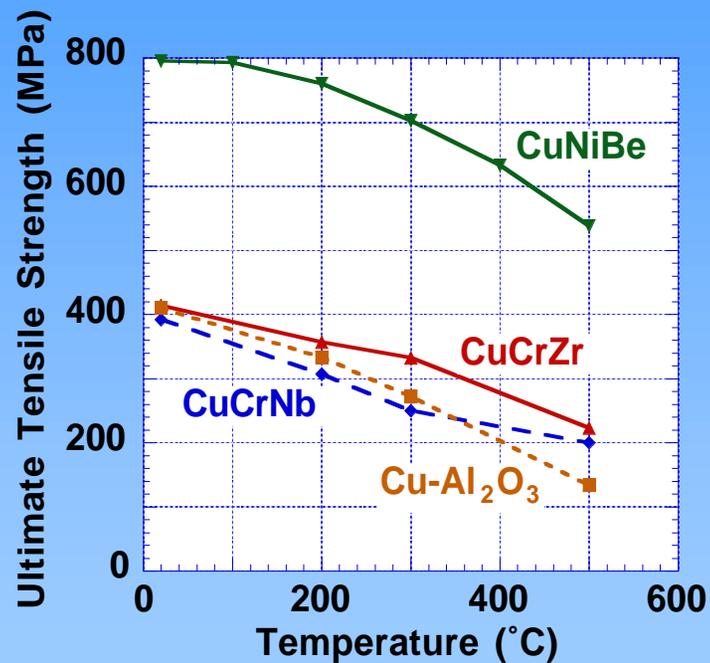


- Suitable insulators are available for fusion reactor applications

Structural Materials will Strongly Impact the Economics of Fusion Energy

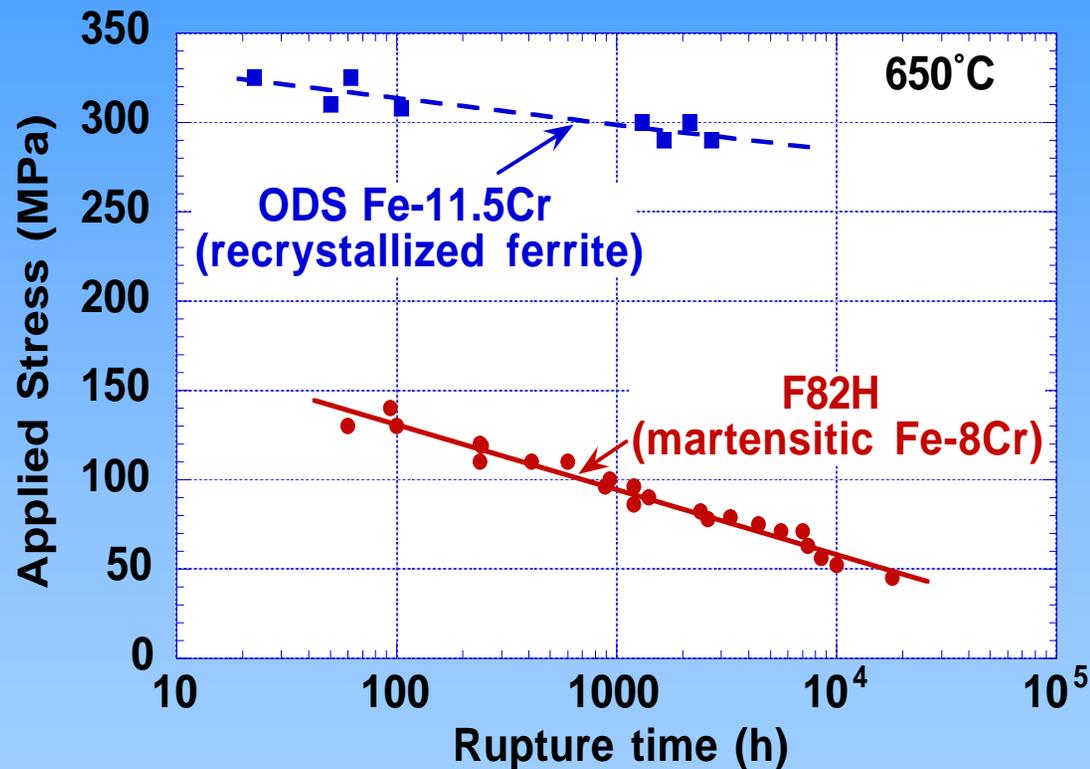
- **Key issues include thermal stress capacity, coolant compatibility, safety, waste disposal, and radiation damage effects**
- **The 3 leading candidates are ferritic/martensitic steel, V alloys, and SiC/SiC**
 - **Ti alloys have high hydrogen (tritium) solubility and permeability, and low thermal stress capacity**
 - **Ni base superalloys have poor radiation stability (grain boundary embrittlement)**
 - **Refractory alloys (Ta, Mo, W) must be operated at very high temperature (>650°C) to avoid radiation embrittlement**

Copper Alloys have High Thermal Stress Capacity at Low Temperatures, but Poor Elevated Temperature ($>300^{\circ}\text{C}$) Mechanical Properties



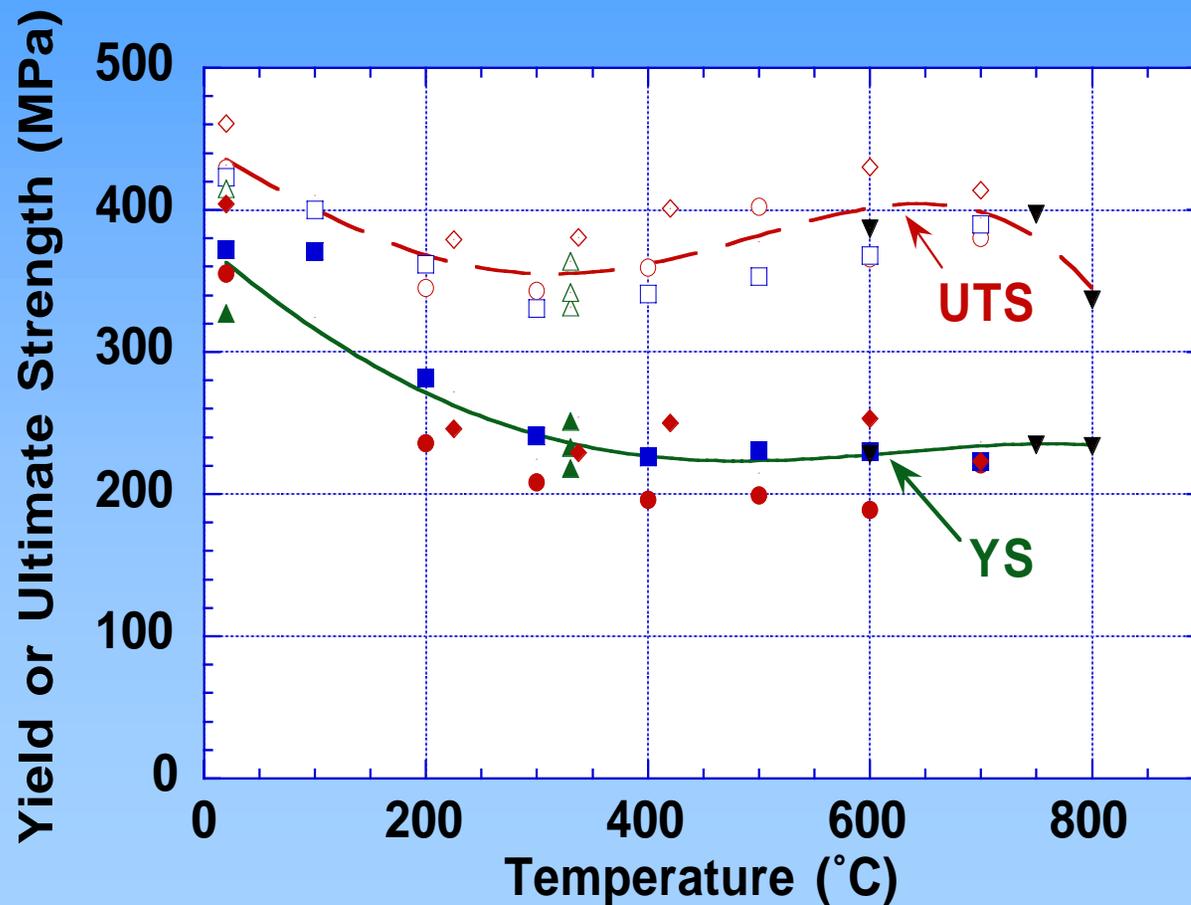
- Copper alloys are not attractive candidates for 1st wall/blanket structural applications (low thermodynamic efficiency)

Recently Developed Isotropic Oxide Dispersion Strengthened Steels Offer Potential for Improved Performance



- Thermal creep temperature limit for martensitic Fe-8Cr steel is ~550°C (vs. >650°C for ODS steel)

V-4Cr-4Ti has an attractive combination of strength, liquid metal compatibility, and high temperature radiation resistance



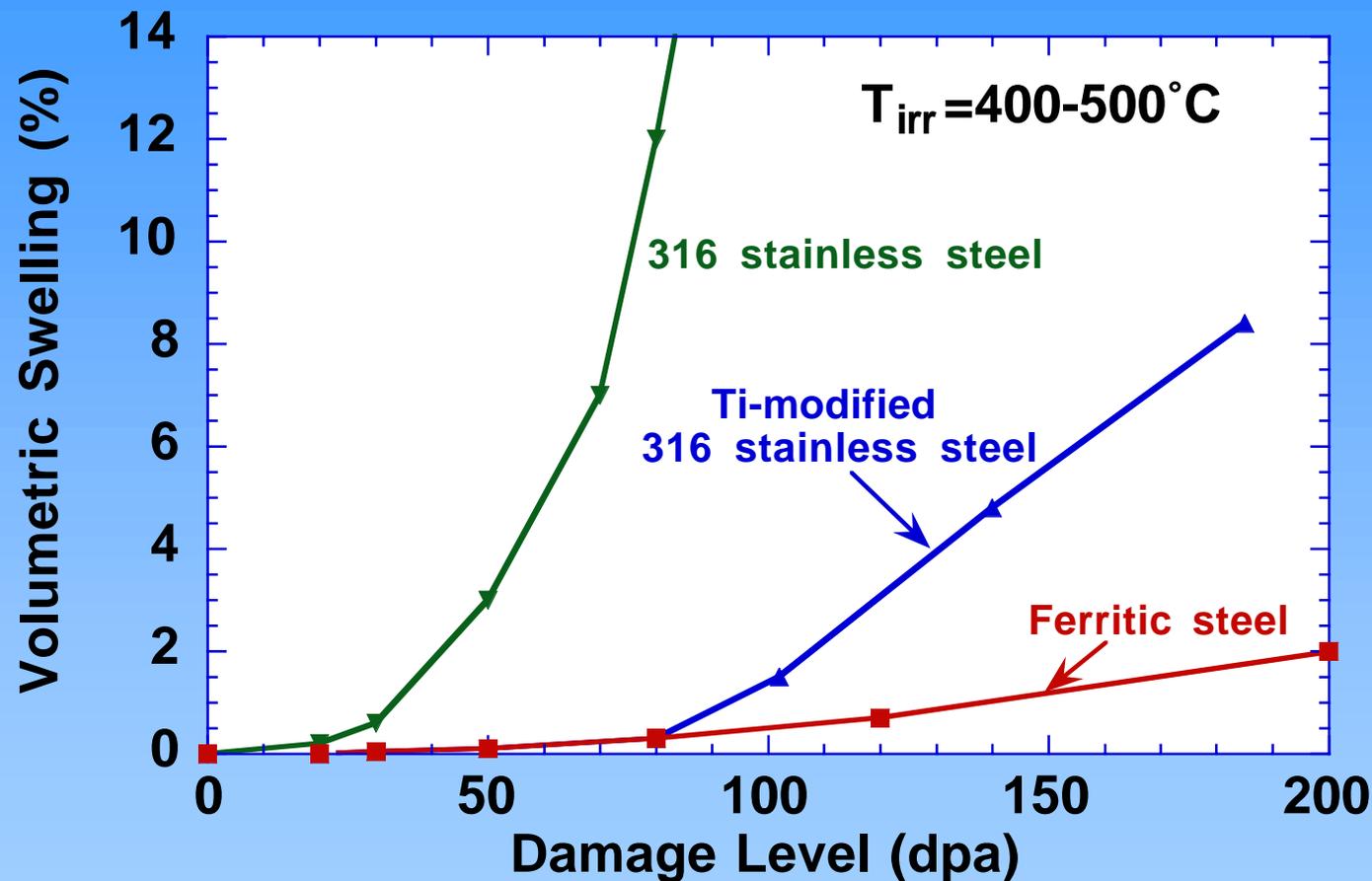
Radiation Damage can Produce Large Changes in Structural Materials

- Radiation hardening and embrittlement ($<0.4 T_M$)
- Irradiation creep ($<0.45 T_M$)
- Volumetric swelling from void formation ($0.3-0.6 T_M$)
- High temperature He embrittlement ($>0.5 T_M$)

In addition...

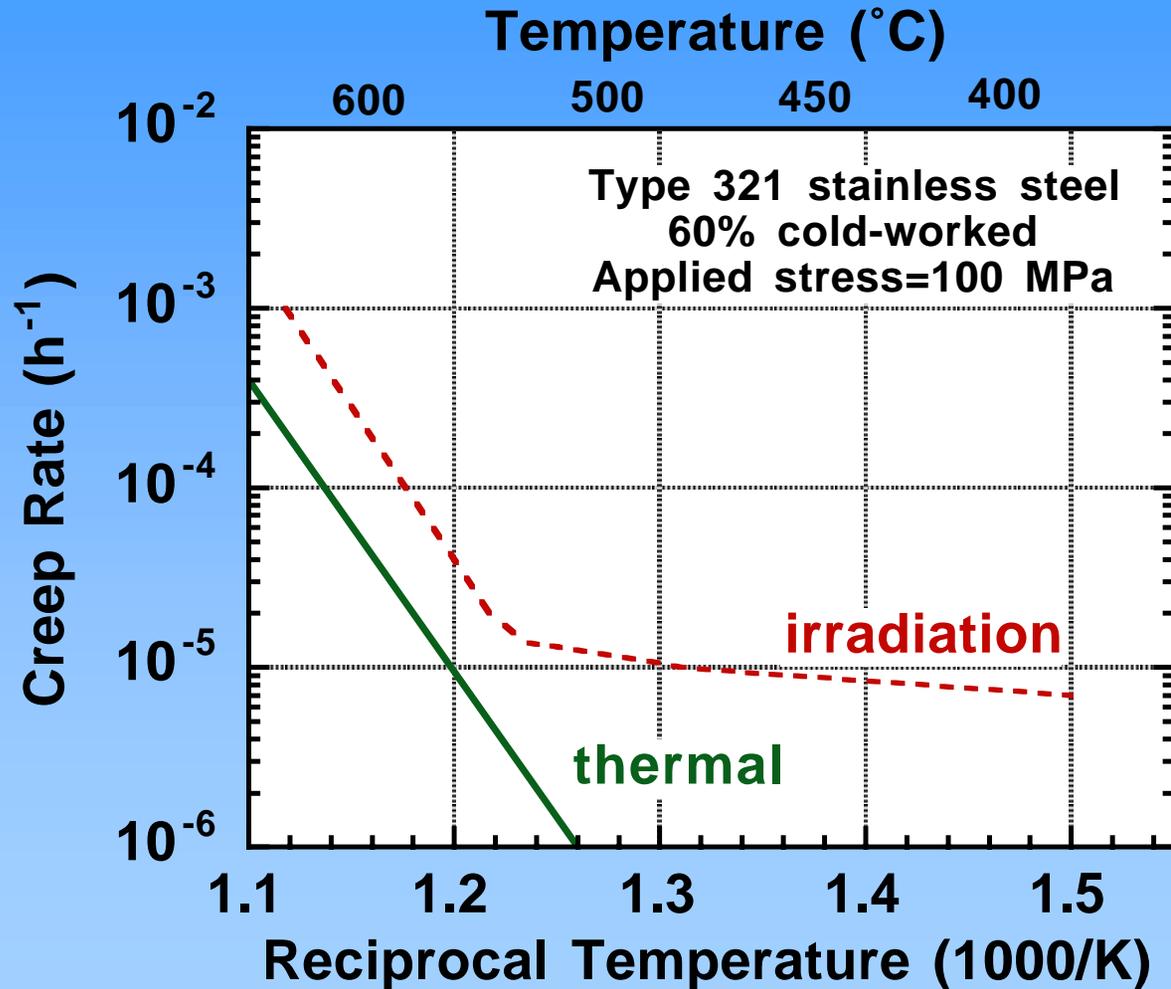
- The irradiation environment associated with a D-T fusion reactor is more severe than in fission reactors
 - Higher lifetime dose requirements for structure
 - Higher He generation rates (promotes He embrittlement of grain boundaries, void swelling)

Swelling resistant alloys have been developed via international collaborations

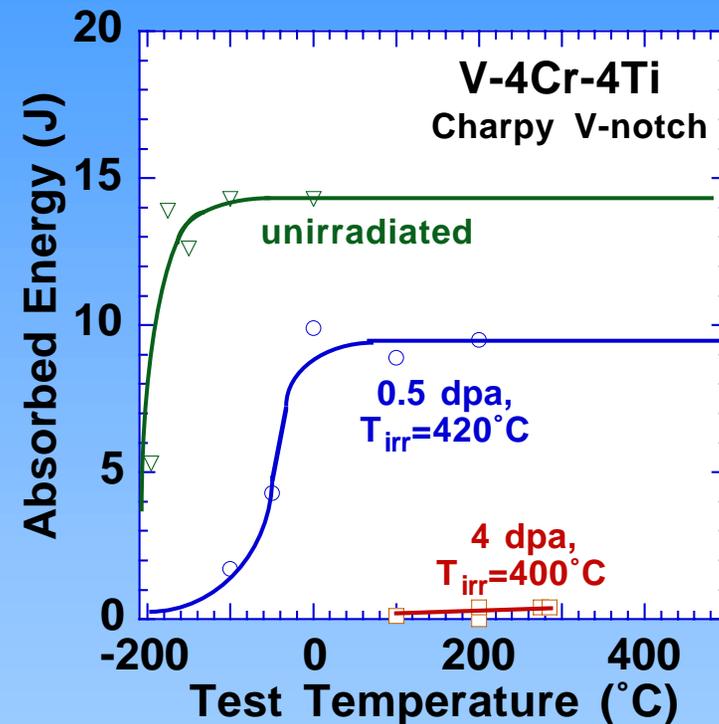
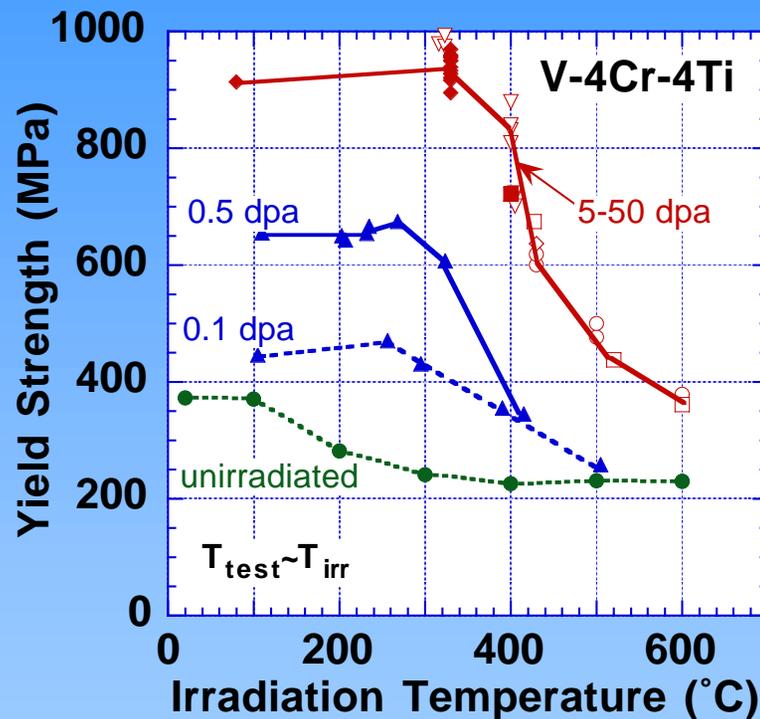


- Lowest swelling is observed in body-centered cubic alloys (V alloys, ferritic steel)

Irradiation Creep Dominates over Thermal Creep below 500°C in Austenitic Steel



Low Temperature Irradiation causes Hardening and Loss of Ductility in Metals



- Matrix hardening produces an increase in the ductile-to-brittle transition temperature in body-centered-cubic alloys (ferritic steels, V alloys)

Summary

- **Impressive physics advances have been achieved from a relatively modest investment**
 - 1950-1995 fusion R&D funding ~5% of **annual** gasoline expenditure by US consumers
- **Several key questions still remain**
 - What is the optimal path for development of a commercially viable power plant (magnetic vs. inertial confinement, etc.)?
 - Can fusion be cost-competitive with coal, fission?
- **Materials will play a major role in determining the fate of fusion energy**
 - Fusion energy economics may require new high heat flux, radiation resistant materials